

OSTROLENK, FABER, GERB & SOFFEN, LLP

Attorneys at Law

1180 Avenue of the Americas  
New York, New York 10036-8403

(212) 382-0700

Telex  
23 6925

Facsimile  
(212) 382-0888

Cable  
Ostrofaber NewYork

Asst. Commissioner of Patents and Trademarks  
Washington, DC 20231

OFGS File No. : P/1071-814  
Inventor : Nobuyuki WADA, et al.  
Title : DIELECTRIC CERAMIC COMPOSITION  
AND LAMINATED CERAMIC CAPACITOR  
USING THE SAME  
Assignee : Murata Manufacturing Co., Ltd.

Enclosed herewith please find the following documents in the above-identified application for United States Letters Patent:

67 Pages of Specification including Abstract and Claims  
20 Numbered Claims Calculated as 20 Claims for Fee Purposes  
5 Sheets of Drawing Containing Figures 1 to 7. (Formal/Informal)  
X Declaration and Power of Attorney (Unsigned)  
X Priority is Claimed under 35 U.S.C. §119:

Convention Date August 11, 1998 for Japanese Appln. S.N. 10-227202

Convention Date August 11, 1998 for Japanese Appln. S.N. 10-227203

X Return-Addressed Post Card

OFGS Check No. 086714, which includes the fee of \$760.00, calculated as follows:

Basic Filing Fee: . . . . . \$ 760.00  
Additional Filing Fees:  
Total Number of Claims in Excess of 20, times \$18: . . . .  
Number of Independent Claims in Excess of 3, times \$78: . .  
One or More Multiple Dependent Claims: Total \$260. . . . .  
Total Filing Fees or . . . . .  
Total Filing Fee Reduced 50% for Small Entity: . . . . .  
Assignment Recording Fee: \$40 . . . . .  
TOTAL Filing Fee and Assignment Recording Fee: . . . . . \$ 760.00

In the event the actual fee is greater than the payment submitted or is inadvertently not enclosed, or if any additional fee during the prosecution of this case is not paid, the Patent and Trademark Office is authorized to charge the underpayment to Deposit Account No. 15-0700.

EXPRESS MAIL CERTIFICATE

Respectfully submitted,

I hereby certify that this correspondence is being deposited with the United States Postal Service as Express Mail Post Office to Addressee (mail label #EL010287643US) in an envelope addressed to: Asst. Commissioner of Patents and Trademarks, Washington, D.C. 20231, on August 6, 1999:

Dorothy Jenkins

Name of Person Mailing Correspondence

*Dorothy Jenkins*

Signature

August 6, 1999

Date of Signature

*Edward A. Meilman*

Edward A. Meilman

Registration No.: 24,735

OSTROLENK, FABER, GERB & SOFFEN, LLP

1180 Avenue of the Americas

New York, New York 10036-8403

Telephone: (212) 382-0700

EAM:mgs

- 1 -

DIELECTRIC CERAMIC COMPOSITION AND  
LAMINATED CERAMIC CAPACITOR USING THE SAME

BACKGROUND OF THE INVENTION

1. Field of the Invention

5           The present invention relates to a dielectric ceramic composition and a laminated ceramic capacitor using the same, especially to a ceramic capacitor having inner electrodes made of Ni.

2. Description of the Related Art

10           Ceramic layers and inner electrode metal layers are alternately stacked in the laminated ceramic capacitor. A cheap base metal such as Ni has been recently used for the inner electrodes in place of expensive noble metals such as Ag and Pd for reducing the  
15           production cost. When Ni is used for the electrodes, the capacitor should be fired in a reducing atmosphere where Ni is not oxidized. However, ceramics comprising barium titanate as a principal component may be endowed with semiconductive properties when the ceramics are fired in  
20           a reducing atmosphere. Accordingly, as disclosed for example in Japanese Examined Patent Publication No. 57-42588, a dielectric material in which the ratio between the barium site and titanium site in the barium titanate solid solution is adjusted to be larger than the  
25           stoichiometric ratio has been developed. This allows the laminated ceramic capacitor using Ni as electrodes to be practically used, thereby expanding its production scale.

          Since electronic parts have been rapidly miniaturized with the recent advance of electronics,

small size ceramic capacitors with large capacitance as well as temperature stability of electrostatic capacitance are required. The ceramic capacitors having the Ni electrodes are also under the same circumstances.

5           For complying with the requirements of large capacitance and small size, the dielectric ceramics should be made to be thinner and multi-layered. However, much higher voltage is impressed on the dielectric material when the dielectric ceramic layer is thinned, 10 often causing troubles such as decrease of dielectric constant, increase of temperature dependency of the electrostatic capacitance and deteriorated stability of other characteristics when conventional dielectric materials are used. Especially, when the thickness of 15 the dielectric layer is reduced to 5  $\mu\text{m}$  or less, 10 or less ceramic particles are contained between the inner electrodes, making it difficult to assure a stable quality.

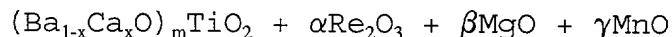
20           Making the dielectric layer thin is accompanied by other problems. Solder plating layers as external electrodes are usually formed on the baked electrodes of a conductive metal powder in order to comply with automatic packaging of the laminated ceramic capacitor. Therefore, the plating layer is generally formed by 25 electroplating. Oxides containing boron or a glass is added, on the other hand, into some dielectric ceramics as a sintering aid. However, the dielectric ceramic using these additives has so poor resistance against plating that characteristics of the laminated ceramic 30 capacitor may be deteriorated by dipping it into a plating solution. It has been a problem that reliability is markedly decreased in the ceramic capacitor having thin dielectric ceramic layers.

SUMMARY OF THE INVENTION

Accordingly, the object of the present invention is to provide a laminated ceramic capacitor with high reliability and large capacitance especially using Ni for inner electrodes, wherein dielectric constant is not decreased exhibiting a stable electrostatic capacitance even when the dielectric ceramic layers are thinned, and temperature characteristics of the electrostatic capacitance satisfy the B-grade characteristics prescribed in the JIS standard and the X7R-grade characteristics prescribed in the EIA standard.

The present invention also provides a highly reliable laminated ceramic capacitor with large capacitance made of thin dielectric ceramic layers having an excellent plating solution resistance.

In one aspect, the present invention provides a laminated ceramic capacitor provided with a plurality of dielectric ceramic layers, inner electrodes formed between the dielectric ceramic layers and external electrodes being in electrical continuity with the inner electrodes, the dielectric ceramic layer being represented by the following formula:



( $\text{Re}_2\text{O}_3$  is at least one or more of the compounds selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$ ,  $\alpha$ ,  $\beta$ ,  $\gamma$ ,  $m$  and  $x$  representing molar ratio in the range of  $0.001 \leq \alpha \leq 0.10$ ,  $0.001 \leq \beta \leq 0.12$ ,  $0.001 < \gamma \leq 0.12$ ,  $1.000 < m \leq 1.035$  and  $0.005 < x \leq 0.22$ ), and containing about 0.2 to 5.0 parts by weight of either a first sub-component or a second sub-component relative to 100 parts by weight of a principal component containing about 0.02% by weight or less of alkali-metal oxides in  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$  as a

starting material to be used for the dielectric ceramic layer, wherein the first sub-component is a  $\text{Li}_2\text{O}-(\text{Si},\text{Ti})\text{O}_2$ -MO based oxide (MO is at least one of the compound selected from  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$ ) and the second sub-component is a  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxide (XO is at least one of the compound selected from BaO, CaO, SrO, MgO, ZnO and MnO). The inner electrodes are preferably composed of nickel or a nickel alloy.

The material  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$  to be used for the dielectric ceramic layer preferably has a mean particle size of about 0.1 to 0.7  $\mu\text{m}$ .

The first sub-component represented by  $x\text{LiO}_2-y(\text{Si}_w\text{Ti}_{1-w})\text{O}_2-z\text{MO}$  (x, y and z are represented by molar percentage (mol%) and w is in the range of  $0.30 \leq w \leq 1.0$ ) may be within the area surrounded by the straight lines connecting between the succeeding two points represented by A (x = 20, y = 80, z = 0), B (x = 10, y = 80, z = 10), C (x = 10, y = 70, z = 20), D (x = 35, y = 45, z = 20), E (x = 45, y = 45, z = 10) and F (x = 45, y = 55, z = 0) or on the lines in a ternary composition diagram having apexes represented by each component  $\text{LiO}_2$ ,  $(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$  and MO provided that when the component is on the line A-F, w is in the range of  $0.3 \leq w < 1.0$ .

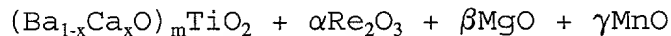
The second sub-component represented by  $x\text{SiO}_2-y\text{TiO}_2-z\text{XO}$  (x, y and z are represented by mol%) may be within the area surrounded by the straight lines connecting between the succeeding two points represented by A (x = 85, y = 1, z = 14), B (x = 35, y = 51, z = 14), C (x = 30, y = 20, z = 50) and D (x = 39, y = 1, z = 60) or on the lines in a ternary composition diagram having apexes represented by each component  $\text{SiO}_2$ ,  $\text{TiO}_2$  and XO.

At least one of the compounds  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  are contained with a combined amount of about 15 parts by weight ( $\text{ZrO}_2$  is about 5 parts by weight or less) in the second sub-component relative to 100 parts by weight of the  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxide.

The external electrodes are composed of sintered layers of a conductive metal powder or a conductive metal powder supplemented with a glass frit.

Alternately, the external electrodes are composed of sintered layers of a conductive metal powder or a conductive metal powder supplemented with a glass frit, and plating layers formed thereon.

It is preferable to use the ceramic having the composition to be described hereinafter in order to improve the plating resistance. The dielectric ceramic layer in the laminated ceramic capacitor is represented by the following formula:



( $\text{Re}_2\text{O}_3$  is at least one or more of the compounds selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$ ,  $\alpha$ ,  $\beta$ ,  $\gamma$ ,  $m$  and  $x$  representing molar ratio in the range of  $0.001 \leq \alpha \leq 0.10$ ,  $0.001 \leq \beta \leq 0.12$ ,  $0.001 < \gamma \leq 0.12$ ,  $1.000 < m \leq 1.035$  and  $0.005 < x \leq 0.22$ ), and contains about 0.2 to 5.0 parts by weight of the compound selected from either a first sub-component, a second sub-component or a third sub-component relative to 100 parts by weight of a principal component containing about 0.02% by weight or less of alkali-metal oxides in  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$  as a starting material to be used for the dielectric ceramic layers, wherein the first sub-component is a  $\text{Li}_2\text{O}$ - $\text{B}_2\text{O}_3$ -(Si, Ti) $\text{O}_2$  based oxide, the second sub-component is a  $\text{Al}_2\text{O}_3$ -MO- $\text{B}_2\text{O}_3$  based oxide (MO is at least one of the

compound selected from BaO, CaO, SrO, MgO, ZnO and MnO) and the third sub-component is SiO<sub>2</sub>.

5           The first sub-component represented by  
xLiO<sub>2</sub>-yB<sub>2</sub>O<sub>3</sub>-z(Si<sub>w</sub>Ti<sub>1-w</sub>)O<sub>2</sub> (x, y and z are represented by  
mol% and w is in the range of 0.30 ≤ w ≤ 1.0) is  
preferably within the area surrounded by the straight  
lines connecting between the succeeding two points  
represented by A (x = 0, y = 20, z = 80), B (x = 19, y =  
1, z = 80), C (x = 49, y = 1, z = 50), D (x = 45, y = 50,  
10   z = 5), E (x = 20, y = 75, z = 5) and F (x = 0, y = 80, z  
= 20) or on the lines in a ternary composition diagram  
having apexes represented by each component LiO<sub>2</sub>, B<sub>2</sub>O<sub>3</sub> and  
(Si<sub>w</sub>Ti<sub>1-w</sub>)O<sub>2</sub>.

15           At least one of the compounds Al<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub> are  
contained in a combined amount of about 20 parts by  
weight or less (ZrO<sub>2</sub> is about 10 parts by weight or less)  
in the first sub-component relative to 100 parts by  
weight of the Li<sub>2</sub>O-B<sub>2</sub>O<sub>3</sub>-(Si, Ti)O<sub>2</sub> based oxide.

20           The second sub-component represented by  
xAl<sub>2</sub>O<sub>3</sub>-yMO-zB<sub>2</sub>O<sub>3</sub> (x, y and z are represented by mol%) is  
preferably within the area surrounded by the straight  
lines connecting between the succeeding two points  
represented by A (x = 1, y = 14, z = 85), B (x = 20, y =  
10, z = 70), C (x = 30, y = 20, z = 50), D (x = 40, y =  
25   50, z = 10), E (x = 20, y = 70, z = 10) and F (x = 1, y =  
39, z = 60) or on the lines in a ternary composition  
diagram having apexes represented by each component Al<sub>2</sub>O<sub>3</sub>,  
yMO and zB<sub>2</sub>O<sub>3</sub>.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a cross section showing one example of the laminated ceramic capacitor according to the present invention.

5            Fig. 2 is a plane view showing the dielectric ceramic layer part having the inner electrodes in the laminated ceramic capacitor shown in FIG. 1.

10           FIG. 3 is a disassembled perspective view showing the laminated ceramic part in the laminated ceramic capacitor shown in FIG. 1.

FIG. 4 is a ternary composition diagram of the  $\text{LiO}_2$ - $(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$ -MO based oxide.

FIG. 5 is a ternary composition diagram of the  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxide.

15           FIG. 6 is a ternary composition diagram of the  $\text{Li}_2\text{O}$ - $\text{B}_2\text{O}_3$ - $(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$  based oxide.

FIG. 7 is a ternary composition diagram of the  $\text{Al}_2\text{O}_3$ -MO- $\text{B}_2\text{O}_3$  based oxide.

#### DESCRIPTION OF THE PREFERRED EMBODIMENT

20           The laminated ceramic capacitor according to the present invention will now be explained in more detail with reference to the accompanying drawings.

25           Fig. 1 is a cross section showing one example of the laminated ceramic capacitor according to the present invention, Fig. 2 is a plane view showing the dielectric ceramic layer part having the inner electrodes in the laminated ceramic capacitor shown in FIG. 1 and FIG. 3 is a disassembled perspective view showing the laminated ceramic part in the laminated ceramic capacitor shown in FIG. 1. In the laminated ceramic capacitor 1 according to the present invention as shown in FIG. 1, outer electrodes 5, and first plating layers 6 and second

30



plating layers 7 if necessary, are formed on both ends of a ceramic laminated body 3 obtained by laminating a plurality of dielectric ceramic layers 2a and 2b via inner electrodes 4.

5                   The dielectric ceramic layers 2a and 2b are composed of a dielectric ceramic composition having as principal components barium calcium titanate ( $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$ , at least one compound selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$ ,  $\text{MgO}$  and  $\text{MnO}$ , and  
10                   containing as sub-components either a  $\text{Li}_2\text{O}-(\text{Si}, \text{Ti})\text{O}_2-\text{MnO}$  based oxide (MO is at least one of the compounds selected from  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$ ) or a  $\text{SiO}_2-\text{TiO}_2-\text{XO}$  based oxide (XO is at least one of the compounds selected from  $\text{BaO}$ ,  $\text{CaO}$ ,  $\text{SrO}$ ,  $\text{MgO}$ ,  $\text{ZnO}$  and  $\text{MnO}$ ). The composition described above  
15                   allows a laminated ceramic capacitor with high reliability and excellent insulating strength to be obtained, wherein the ceramic capacitor can be fired without endowing it with semiconductive properties even by firing in a reducing atmosphere, the temperature  
20                   characteristics of the electrostatic capacitance satisfy the B-grade characteristics prescribed in the JIS standard and the X7R-grade characteristics prescribed in the EIA standard and the ceramic capacitor has a high insulation resistance at room temperature and at high  
25                   temperatures.

                  Also, a highly reliable laminated ceramic capacitor, whose dielectric constant is less affected by variation of electric field even when the dielectric ceramic layers are thinned and magnetic field strength is  
30                   increased, can be obtained by using a barium calcium titanate material with a mean particle size of about 0.1 to 0.7  $\mu\text{m}$ . The dielectric ceramic assumes a core-shell structure in which Re components (Re is at least one or

more of the elements selected from Y, Gd, Tb, Dy, Ho, Er and Yb) are distributed in the vicinity of and at grain boundaries by diffusion during firing.

5 A highly reliable dielectric material can be also obtained by using a barium calcium titanate containing about 0.02% by weight or less of alkali metal oxides such as  $\text{Na}_2\text{O}$  and  $\text{K}_2\text{O}$ .

10 The ratio (n) of (barium + calcium)/titanium in the barium calcium titanate material is not specifically limited. However, the ratio (n) in the range from about 0.990 to 1.035 is desirable when stability for producing powder materials is taken into consideration.

15  $\text{Li}_2\text{O}-(\text{Si}, \text{Ti})\text{O}_2-\text{MO}$  based oxides contained in the principal components described above serve for firing the dielectric ceramics at a relatively low temperature of  $1250^\circ\text{C}$ , improving high temperatures load characteristics.  $\text{SiO}_2-\text{TiO}_2-\text{XO}$  based oxides included in the principal components also allow the sintering property to be excellent along with improving the voltage load  
20 characteristics at a high temperature and humidity. Further, a higher insulation resistance can be obtained by allowing  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  to be contained in the  $\text{SiO}_2-\text{TiO}_2-\text{XO}$  based oxides.

25 The inner electrode 4 is composed of base metals such as nickel or a nickel alloy.

30 The outer electrode 5 is composed of a sintered layer of various conductive metals such as Ag, Pd, Ag-Pd, Cu or a Cu alloy, or a sintered layer prepared by blending the foregoing conductive metal powder with various glass frits such as  $\text{B}_2\text{O}_3-\text{Li}_2\text{O}-\text{SiO}_2-\text{BaO}$  based,  $\text{B}_2\text{O}_3-\text{SiO}_2-\text{BaO}$  based,  $\text{Li}_2\text{O}-\text{SiO}_2-\text{BaO}$  based or  $\text{B}_2\text{O}_3-\text{SiO}_2-\text{ZnO}$  based glass frit. It is possible to form a plating layer on this sintered layer. Either a first plating layer 6

comprising Ni, Cu or a Ni-Cu alloy may be merely formed or a second plating layer 7 comprising tin or a solder may be formed on the first plating layer.

5 The method for producing the laminated ceramic capacitor according to the present invention will be described hereinafter in the order of its production steps with reference to FIGS. 1 to 3.

10 Powder materials produced by a solid phase method for allowing oxides and carbonates to react at a high temperature or a powder material produced by a wet synthesis method such as a hydrothermal synthesis method or alkoxide method are prepared as starting materials of the dielectric ceramics. A solution of an alkoxide or an organometallic compound may be used for the additives  
15 other than oxides and carbonates.

20 After weighing the prepared materials in a prescribed composition ratio with mixing, the mixed powder is turned into a slurry by adding an organic binder to obtain a green sheet (the dielectric ceramic layers 2a and 2b) by molding the slurry into a sheet. The inner electrodes 4 comprising nickel or a nickel alloy are then formed on one face of the green sheet (the dielectric ceramic layers 2b). Any method including screen printing, vacuum deposition or plating may be used  
25 for forming the inner electrodes 4.

30 Then, a required number of the green sheets (the dielectric ceramic layers 2b) having the inner electrodes 4 are laminated, which are inserted between the green sheets having no inner electrodes (the dielectric ceramic layers 2a) to form a laminated body after pressing. A ceramic laminated body 3 is obtained by firing the laminated body at a given temperature in a reducing atmosphere.

A pair of the outer electrodes 5 are formed on both side ends of the ceramic laminate body 3 so as to be in electrical continuity with the inner electrodes 4.

While the outer electrodes 5 are usually formed by coating the metal powder paste on the ceramic laminated body 3 obtained by firing and baking the paste, the outer electrode may be formed simultaneously with forming the ceramic laminated body 3 by coating the paste prior to firing.

Finally, the first plating layer 6 and the second plating layer 7 are formed, if necessary, on the outer electrodes 5, thereby completing the laminated ceramic capacitor 1.

#### Examples

##### Example 1

Starting materials  $\text{TiO}_2$ ,  $\text{BaCO}_3$  and  $\text{CaCO}_3$  are at first prepared. After mixing and crushing the materials, the mixture is heated at  $1000^\circ\text{C}$  or more to synthesize nine kinds of barium calcium titanate shown in TABLE 1. The mean particle size was determined by observing the particles of the material under a scanning electron microscope.

Table 1				
Kind of Barium Calcium Titanate	$(\text{Ba}_{1-x}\text{Ca}_x\text{O})_n\text{TiO}_2$	$(\text{Ba}+\text{Ca})/\text{Ti}_n$	Content of Alkali Metal Oxide Impurities (% by weight)	Mean Particle Size ( $\mu\text{m}$ )
A	0.003	1.000	0.003	0.50
B	0.100	1.000	0.010	0.50
C	0.200	0.998	0.012	0.50
D	0.250	0.998	0.015	0.50
E	0.100	1.000	0.062	0.50
F	0.080	1.005	0.003	0.15
G	0.100	1.008	0.020	0.25
H	0.100	1.000	0.010	0.75
I	0.100	1.000	0.010	0.08

Oxides, carbonates and hydroxides of respective components of the first sub-component were weighed so as to be a composition (molar) ratio of  $0.25\text{Li}_2\text{O}-0.65(0.30\text{TiO}_2-0.70\text{SiO}_2)-0.10\text{Al}_2\text{O}_3$  and the mixture was crushed to obtain a powder. Likewise, oxides, carbonates and hydroxides of respective components of the second sub-component were weighed so as to be a composition ratio of  $0.66\text{Si}_2\text{O}-0.17\text{TiO}_2-0.15\text{BaO}-0.02\text{MnO}$  (molar ratio) and the mixture was crushed to obtain a powder. Then, after heating the powders of the first and second sub-components to  $1500^\circ\text{C}$  in different crucibles, respectively, they were quenched and crushed to obtain respective oxide powders with a mean particle size of  $1\mu\text{m}$  or less.

In the next step,  $\text{BaCO}_3$  or  $\text{TiO}_2$  for adjusting the molar ratio  $m$  of  $(\text{Ba}, \text{Ca})/\text{Ti}$  in the barium calcium titanate, and  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$ ,  $\text{Yb}_2\text{O}_3$ ,  $\text{MgO}$  and  $\text{MnO}$  with purity of 99% or more were prepared. These powder materials and the foregoing oxide powders

for the first and second sub-components were weighed to be the compositions shown in TABLE 2. The amount of addition of the first and second sub-components are given in parts by weight relative to 100 parts by weight of the principal component, i.e.,  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2 + \alpha\text{Re}_2\text{O}_3 + \beta\text{MgO} + \gamma\text{MnO}$ . A polyvinyl butylal based binder and an organic solvent such as ethanol were added to the weighed materials and the mixture was wet-milled with a ball-mill to prepare a ceramic slurry. This ceramic slurry was formed into a sheet by a doctor blade method, obtaining a rectangular green sheet with a thickness of  $4.5\ \mu\text{m}$ . Then, a conductive paste mainly containing Ni was printed on the ceramic green sheet to form conductive paste layers constituting the inner electrodes.

TABLE 2

TABLE 2														
[Ba <sub>1-x</sub> CaxO] <sub>m</sub> •TiO <sub>2</sub> + α Re <sub>2</sub> O <sub>3</sub> + β MgO + γ MnO														
Sample No	Kind of Barium Calcium Titanate	X	m	α							β	γ	The First Sub-Component (parts by weight)	The Second Sub-Component (parts by weight)
				Y <sub>2</sub> O <sub>3</sub>	Gd <sub>2</sub> O <sub>3</sub>	Tb <sub>2</sub> O <sub>3</sub>	Dy <sub>2</sub> O <sub>3</sub>	Ho <sub>2</sub> O <sub>3</sub>	Er <sub>2</sub> O <sub>3</sub>	Yb <sub>2</sub> O <sub>3</sub>				
*1	A	0.003	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
*2	D	0.250	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
*3	B	0.100	1.01	0	0	0	0.0005	0	0	0	0.02	0.005	1	0
*4	B	0.100	1.01	0	0	0	0.11	0	0	0	0.02	0.005	1	0
*5	B	0.100	1.01	0	0	0	0.02	0	0	0	0.0008	0.005	1	0
*6	B	0.100	1.01	0	0	0	0.02	0	0	0	0.13	0.005	1	0
*7	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.0008	1	0
*8	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.13	1	0
*9	B	0.100	0.995	0	0	0	0.02	0	0	0	0.02	0.005	1	0
*10	B	0.100	1	0	0	0	0.02	0	0	0	0.02	0.005	1	0
*11	B	0.100	1.036	0	0	0	0.02	0	0	0	0.02	0.005	1	0
*12	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	0	0
*13	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.1	0	0
*14	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	5.5	0
*15	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	0	5.5
*16	E	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
17	H	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
18	I	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
19	G	0.100	1.025	0.025	0	0	0	0	0	0	0.02	0.005	0	1
20	G	0.100	1.02	0	0.08	0	0	0	0	0	0.05	0.008	4	0
21	G	0.100	1.015	0	0	0.05	0	0	0	0	0.05	0.005	3	0
22	B	0.100	1.01	0	0	0	0	0.02		0	0.02	0.05	2	0
23	B	0.100	1.01	0	0	0	0	0	0.02	0	0.02	0.05	0	1
24	C	0.200	1.005	0	0	0	0	0	0	0.03	0.02	0.05	0	1
25	C	0.200	1.005	0.005	0	0	0.02	0	0	0	0.02	0.005	0	1
26	F	0.080	1.015	0.005	0.015	0	0	0	0	0	0.02	0.005	2	0
27	F	0.080	1.015	0	0	0	0.02		0	0	0.02	0.005	0	2

\* The samples marked (\*) are out of the range of the present invention.

Next, a plurality of ceramic green sheets on which the conductive paste layers had been formed were laminated to obtain a laminated body so that the sides where the conductive paste layers are exposed alternately come to the opposite ends. The laminated body was heated at a temperature of 350°C in a N<sub>2</sub> atmosphere. After driving out the binder, the laminated body was fired in a reducing atmosphere comprising a H<sub>2</sub>-N<sub>2</sub>-H<sub>2</sub>O gas with an oxygen partial pressure of 10<sup>-9</sup> to 10<sup>-12</sup> MPa to obtain a ceramic sintered body.

After firing, an Ag paste containing a B<sub>2</sub>O<sub>3</sub>-Li<sub>2</sub>-SiO<sub>2</sub>-BaO based glass frit was coated on both side faces of the ceramic sintered body, which was baked at a temperature of 600°C in the N<sub>2</sub> atmosphere to form the outer electrodes electrically connected to the inner electrodes.

The laminated ceramic capacitor thus obtained had an overall dimension with a width of 5.0 mm, a length of 5.7 mm and a thickness of 2.4 mm with a thickness of the dielectric ceramic layers inserted between the inner electrodes of 3 μm. The total number of the effective dielectric ceramic layers was five with a confronting electrode area per layer of 16.3 × 10<sup>-6</sup> m<sup>2</sup>.

Electric characteristics of these laminated ceramic capacitors were then determined. Electrostatic capacitances and dielectric losses (tan δ) were measured per JIS C5102 standard using an automatic bridge type measuring apparatus and dielectric constant was calculated from the electrostatic capacitance obtained. Insulation resistance was also measured using an insulation resistance meter by impressing a direct-current voltage of 10 V for 2 minutes to calculate resistivity (ρ).



DV vias characteristics were also measured. The electrostatic capacitance was determined while impressing a direct-current voltage of 15 V (5 kV/mm) and the rate of change of the electrostatic capacitance ( $\Delta C$  %) was determined relative to the electrostatic capacitance measured without impressing a direct-current voltage.

The rate of temperature dependent change of the electrostatic capacitance was also measured. The maximum value of the rate of change in the temperature range from  $-25^{\circ}\text{C}$  to  $85^{\circ}\text{C}$  relative to the capacitance at  $20^{\circ}\text{C}$  ( $\Delta C/C_{20}$ ) and the maximum value of the rate of change in the temperature range from  $-55^{\circ}\text{C}$  to  $125^{\circ}\text{C}$  relative to the capacitance at  $25^{\circ}\text{C}$  ( $\Delta C/C_{25}$ ) were determined with respect to the rate of change of the capacitance.

A high temperature load test was carried out by measuring the time dependent changes of the insulation resistance when a direct-current voltage of 30 V was impressed at  $150^{\circ}\text{C}$ . Lifetime of each sample was defined to be the time when the insulation resistance of each sample had decreased to  $10^5 \Omega$  or less, and a mean lifetime was determined using a plurality of the samples.

The dielectric breakdown voltage was measured by impressing DC voltages with a voltage increasing rate of 100 V/sec. The results are summarized in TABLE 3.

TABLE 3

Sample No	Burning Temp (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance		Rate of Temperature Dependent Change of Capacitance		Resistivity $\rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage		Mean Lifetime (h)		
				$\Delta C$ %	DC	$\Delta C/C20$ %	$\Delta C/C25$ %		$\log \rho$	DC			
												5Kv/mm	-55~+125°C
*1	1300	3360	4.5	-65		-9.7	-15.6	13.2	14	3			
*2	1250	1130	9.3	-35		-4.5	-6.5	13.1	15	23			
*3	1250	2430	4.6	-55		-1.5	-10.6	13.2	14	2			
*4	1250	1220	3.1	-37		-18.1	-23.3	13.5	15	15			
*5	1250	2570	3.6	-63		-15.6	-24.7	12.9	12	65			
*6	1350	1780	4.4	-45		-7.8	-14.6	13.1	14	2			
*7	1250	1950	4.7	-57		-9.6	-15.4	11.8	14	17			
*8	1250	1730	3.8	-56		-13.6	-19.7	11.2	14	8			
*9	1250	2100	5.6	-60		-12.3	-18.6	11.2	8	-			
*10	1250	2060	5.3	-62		-12.2	-17.5	11.6	9	-			
*11	1300	1950	4.4	-50		-8.6	-14.4	12.3	9	1			
*12	1350	1530	5.1	-45		-8.8	-13.7	11.4	10	-			
*13	1350	1470	5.3	-47		-8.9	-14.2	11.5	9	-			
*14	1200	1680	3.2	-48		-14.5	-30.6	13.1	14	5			
*15	1200	1740	3.4	-42		-13.3	-26.8	13.1	14	3			
*16	1250	1750	3.7	-48		-10.5	-15.1	13.1	14	21			
17	1250	2370	4.7	-51		-4.7	-6.7	13.1	13	52			
18	1150	1040	2.5	-30		-8.4	-14.2	13.5	15	174			
19	1175	1410	2.2	-35		-9.6	-14.4	13.2	14	85			
20	1150	1260	2.3	-33		-8.8	-13.7	13.2	15	110			
21	1175	1260	2.3	-36		-9.2	-14.6	13.2	14	105			
22	1200	1900	2.1	-42		-8.6	-13.4	13.2	14	85			
23	1250	2010	2.5	-44		-8.5	-13.8	13.2	15	80			
24	1250	1430	1.8	-34		-7.8	-11.4	13.1	14	110			
25	1250	1450	1.9	-31		-8.2	-11.1	13.2	15	120			
26	1175	1260	1.7	-32		-9.5	-14.5	13.2	14	92			
27	1175	1340	1.6	-33		-9.2	-13.5	13.2	14	95			

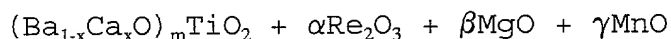
\* The samples marked by (\*) are out of the range of the present invention.

The cross section of the laminated ceramic capacitor obtained was polished and subjected to chemical etching. It was found from scanning electron microscopic observation of the grain size in the dielectric ceramics that the grain size was almost equal to the particle size of the barium calcium titanate starting material in the samples having the compositions within the range of the present invention.

As are evident from TABLE 1 to TABLE 3, the rate of temperature dependent change of the electrostatic capacitance satisfies the B-grade characteristic standard prescribed in the JIS standard in the temperature range from -25°C to +85°C, along with satisfying the X7R-grade characteristic standard prescribed in the EIA standard in the temperature range from -55°C to +125°C, in the laminated ceramic capacitor according to the present invention. In addition, the rate of change of the capacitance when a DC voltage of 5 kV/mm is impressed is as small as within 51%, the change of the electrostatic capacitance being also small when the capacitor is used has thin layers. Moreover, the mean lifetime in the high temperature load test is as long as 52 hours or more, enabling one to fire at a firing temperature of 1250°C or below.

The reason why the compositions are limited in the present invention will be described hereinafter.

In the composition represented by the following formula:



( $\text{Re}_2\text{O}_3$  represents at least one of the compounds selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$  and  $\alpha$ ,  $\beta$  and  $\gamma$  represent molar ratios), a CaO content (x) of about 0.005 or less as in the sample No. 1 is not preferable

since the rate of impressed voltage dependent change of the capacitance becomes large and the mean lifetime becomes extremely short. It is also not preferable that the CaO content (x) exceeds about 0.22 as in the sample No. 2 because the dielectric loss is increased. Accordingly, the preferable CaO content (x) is in the range of  $0.005 < x \leq 0.22$ .

A  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) of less than about 0.001 as in the sample No. 3 is also not preferable because the mean lifetime becomes extremely short. It is also not preferable that the content of  $\text{Re}_2\text{O}_3$  ( $\alpha$ ) exceed about 0.10 since the temperature characteristics do not satisfy the B/X7R-grade characteristics while the mean lifetime is shortened. Accordingly, the preferable  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) is in the range of  $0.001 \leq \alpha \leq 0.10$ .

A MgO content ( $\beta$ ) of less than about 0.001 as in the sample No. 5 is also not preferable because the rate of impressed voltage dependent change of the capacitance becomes large while the temperature characteristics do not satisfy the B/X7R-grade characteristics. It is also not preferable that the amount of addition ( $\beta$ ) of MgO exceed about 0.12 as in the sample No. 6 since the sintering temperature becomes high to extremely shorten the mean lifetime. Accordingly, the preferable MgO content ( $\beta$ ) is in the range of  $0.001 \leq \beta \leq 0.12$ .

A MnO content ( $\gamma$ ) of less than about 0.001 as in the sample No. 7 is also not preferable because the capacitance is lowered while the mean lifetime is shortened. It is also not preferable that the MnO content ( $\gamma$ ) exceed about 0.12 as in the sample No. 8 since the temperature characteristics do not satisfy the B/X7R-grade characteristics, the resistivity becomes low

and the mean lifetime is shortened. Accordingly, the preferable range of the MnO content ( $\gamma$ ) is  $0.001 < \gamma \leq 0.12$ .

5 It is not preferable that the ratio (m) of (Ba, Ca)/Ti is less than about 1.000 as in the samples No. 9 and No. 10 because the temperature characteristics do not satisfy the B/X7R-grade characteristics, thereby lowering the resistivity besides immediately causing short circuit troubles when a voltage is impressed in the high  
10 temperature load test. It is also not preferable that the ratio (m) of (Ba, Ca)/Ti exceed about 1.035 as in the sample No. 11 because sintering is insufficient to extremely shorten the mean lifetime. Accordingly, the preferable ratio (m) of (Ba, Ca)/Ti is in the range of  
15  $1.000 < m \leq 1.035$ .

It is not preferable that the contents of the first and second sub-components are zero as in the samples No. 12 and No. 13 because the resistivity is lowered to immediately cause short circuit troubles when  
20 a voltage is impressed in the high temperature load test. It is also not preferable that the contents of the first and second sub-components exceed about 5.0 parts by weight as in the sample Nos. 14 and 15 because the second phase based on glass components is increased and the  
25 temperature characteristics do not satisfy the B/X7R-grade characteristics and the mean lifetime is extremely shortened. Accordingly, the preferable content of either the first component or the second component is in the range of about 0.2 to 5.0 parts by weight.

30 The content of the alkali metal oxides contained in barium calcium titanate as impurities is adjusted to about 0.02% by weight or less because, when the content of the alkali metal oxides exceeds about

0.02% by weight as in the sample No. 16, the mean lifetime is shortened.

5 The sample No. 17 in which the mean particle size of barium calcium titanate exceeds  $0.7 \mu\text{m}$  shows a little poor mean lifetime of 52 hours. The sample No. 18 in which the mean particle size of barium calcium titanate is less than  $0.1 \mu\text{m}$  shows, on the other hand, a little small dielectric constant of 1040. Accordingly, the preferable mean particle size of barium calcium  
10 titanate is in the range from about  $0.1$  to  $0.7 \mu\text{m}$ .

#### Example 2

A dielectric powder material represented by the following formula was prepared using the barium calcium titanate (B) in TABLE 1:

15  $(\text{Ba}_{0.90}\text{Ca}_{0.10}\text{O})_{1.010} \cdot \text{TiO}_2 + 0.02\text{Dy}_2\text{O}_3 + 0.02\text{MgO} + 0.010\text{MnO}$  (molar ratio)

A laminated ceramic capacitor was produced by the same method as used in Example 1, except that a  $\text{Li}_2\text{O}-(\text{Si},\text{Ti})\text{O}_2$ -MO based oxide as the first sub-component  
20 having a mean particle size of  $1 \mu\text{m}$  listed in TABLE 4 was added to the mixture above. The size and shape of the laminated ceramic capacitor produced in this example were the same as those in Example 1. The electric characteristic were measured by the same method as used  
25 in Example 1. The results are shown in TABLE 5.

TABLE 4						
Sample. No.	First Subcomponent					
	Amount of addition (parts by weight)	Composition (mol%, except w)				
		Li <sub>2</sub> O	(Si <sub>w</sub> Ti <sub>1-w</sub> )	w	Al <sub>2</sub> O <sub>3</sub>	ZrO <sub>2</sub>
101	1	20	80	0.3	0	0
102	1	10	80	0.6	5	5
103	1	10	70	0.5	20	0
104	2	35	45	1	10	10
105	2	45	35	0.5	10	0
106	2	45	55	0.3	0	0
107	1.5	20	70	0.6	5	5
108	1.5	20	70	0.4	10	0
109	2	30	60	0.7	5	5
110	2	30	60	0.8	10	0
111	2	40	50	0.6	5	5
112	2	40	50	0.9	5	10
113	2	10	85	0.4	5	0
114	2	5	75	0.6	10	10
115	3	20	55	0.5	25	0
116	3	45	40	0.8	0	15
117	3	50	45	0.7	5	0
118	2	25	75	0.9	0	0
119	2	25	75	1	0	0
120	2	45	65	0.9	0	0
121	2	35	65	1	0	0
122	1	20	70	0.2	0	10

TABLE 5

Sample No	Burning Temp (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance		Rate of Temperature Dependent Change of Capacitance		Resistivity		Dielectric Breakdown Voltage		Mean Lifetime (h)
				$\Delta C\%$	DC 5Kv/mm	$\Delta C/C20\%$ -25~+85°C (%)	$\Delta C/C25\%$ -55~+125°C (%)	Log $\rho$ ( $\Omega \cdot \text{cm}$ )	DC (kV/mm)	DC		
101	1250	1920	2.4	-43	-8.2	-12.8	13.2	14	14	82		
102	1250	1910	2.4	-42	-7.8	-12.6	13.1	15	15	86		
103	1250	1870	2.5	-41	-7.7	-12.3	13.2	14	14	84		
104	1225	1850	2.4	-41	-7.5	-12.5	13.5	15	15	88		
105	1225	1870	2.4	-42	-7.2	-11.7	13.2	14	14	90		
106	1225	1870	2.4	-40	-7.8	-12.0	13.1	14	14	80		
107	1250	1910	2.4	-42	-8.1	-12.1	13.3	14	14	85		
108	1250	1910	2.3	-42	-7.8	-11.8	13.2	14	14	90		
109	1225	1890	2.5	-41	-7.7	-11.7	13.3	14	14	90		
110	1225	1900	2.5	-42	-7.9	-12.1	13.2	14	14	95		
111	1225	1890	2.4	-42	-7.8	-12.1	13.2	15	15	91		
112	1225	1850	2.3	-40	-7.6	-11.8	13.3	14	14	87		
113	1300	1620	2.2	-42	-7.9	-12.2	11.5	9	9	-		
114	1300	1460	2.4	-41	-8.0	-12.6	10.8	8	8	-		
115	1300	1330	2.6	-42	-7.8	-12.5	10.6	8	8	-		
116	1300	1420	2.8	-43	-7.8	-12.2	10.8	8	8	-		
117	1300	1360	2.4	-43	-8.6	-12.4	11.2	8	8	-		
118	1250	1920	2.3	-43	-7.8	-11.7	13.2	15	15	88		
119	1300	1450	2.1	-40	-8.2	-11.6	11.1	9	9	-		
120	1250	1900	2.5	-42	-7.6	-11.7	13.2	14	14	88		
121	1300	1350	2.1	-44	-8.5	-12.8	10.2	8	8	-		
122	1350	1420	2.1	-44	-8.2	-11.5	10.2	8	8	-		

- : Measurement is Impossible



As are evident from Table 4 and Table 5, the sample Nos. 101 to 112, 118 and 120, in which  $\text{Li}_2\text{O}-(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$ -Mo based oxides with compositions within the area surrounded by the straight lines connecting

5 between the succeeding two points represented by A ( $x = 20, y = 80, z = 0$ ), B ( $x = 10, y = 80, z = 10$ ), C ( $x = 10, y = 70, z = 20$ ), D ( $x = 35, y = 45, z = 20$ ), E ( $x = 45, y = 45, z = 10$ ) and F ( $x = 45, y = 55, z = 0$ ) (and where  $w$  is in the range of  $0.3 \leq w < 1.0$  when the

10 composition is on the line A-F) or on the lines in a ternary composition diagram having apexes represented by each component  $\text{LiO}_2$ ,  $(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$  and MO ( $x, y$  and  $z$  are represented by mol% and  $w$  is in the range of  $0.3 \leq w \leq 1.0$  when the component is on the line A-F,) are added,

15 has a dielectric constant of as large as 1850, the rate of temperature dependent changes of the electrostatic capacitance satisfy the B-grade characteristic standard prescribed in the JIS standard in the temperature range from  $-25^\circ\text{C}$  to  $+85^\circ\text{C}$ , and satisfy the X7R-grade

20 characteristic standard prescribed in the EIA standard in the temperature range from  $-55^\circ\text{C}$  to  $+125^\circ\text{C}$ . In addition, the rate of change of the capacitance when a DC voltage of 5 kV/mm is impressed is as small as within 43%, the change of the electrostatic capacitance being small when

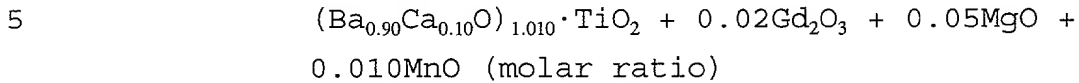
25 used as thin layers. The mean lifetime under the high temperature load test is as long as 80 hours or more, enabling a firing temperature of  $1250^\circ\text{C}$ .

When the compositions of the  $\text{Li}_2\text{O}-(\text{Si}, \text{Ti})\text{O}_2$ -Mo based oxides are out of the range of the present

30 invention as in the sample Nos. 113 to 117, 119, 121 and 122, on the contrary, sintering is insufficient to immediately cause short circuit troubles in the high temperature load test.

Example 3

A dielectric powder material represented by the following formula was prepared using barium calcium titanate in TABLE 1-B:



Laminated ceramic capacitors were produced by the same method as used in Example 1, except that  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxides as the second sub-components (including those supplemented with  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$ ) as shown in TABLE 6 with a mean particle size of 1  $\mu\text{m}$  or less produced by heating at 1200 to 1500°C were added to the powder material above. The size and shape of the laminated ceramic capacitors produced are the same as in Example 1. Electric characteristics were measured by the same method as used in Example 1. The results are shown in TABLE 7.

TABLE 6														
Sample No.	Second Sub-Component													
	Amount of Addition (parts by weight)	Composition (mol%)										Additive Parts by Weight		
		SiO <sub>2</sub>	TiO <sub>2</sub>	BaO	CaO	SrO	MgO	ZnO	MnO	Total	Al <sub>2</sub> O <sub>3</sub>			ZrO <sub>2</sub>
201	1	85	1	1	0	0	0	4	9	14	0	0		
202	1	35	51	0	10	0	0	0	4	14	0	0		
203	1	30	20	0	30	0	15	4	1	50	0	0		
204	1	39	1	20	20	2	0	13	5	60	0	0		
205	1	70	10	5	5	0	0	10	0	20	0	0		
206	1	45	10	0	0	0	0	15	30	45	0	0		
207	1	50	20	10	10	3	7	0	0	30	0	0		
208	1	50	30	0	16	0	0	0	4	20	0	0		
209	1	35	30	25	10	0	0	0	0	35	0	0		
210	1	40	40	10	0	0	0	5	5	20	0	0		
211	1	45	22	3	30	0	0	0	0	33	15	0		
212	1	45	22	3	30	0	0	0	0	33	10	5		
213	1	65	25	5	5	0	0	0	0	10	0	0		
214	1	25	40	15	0	10	0	5	5	35	0	0		
215	1	30	10	30	25	0	0	5	0	60	0	0		
216	1	50	0	35	15	0	0	0	0	50	0	0		
217	1	45	22	30	0	0	3	0	0	33	25	0		
218	1	45	22	30	0	3	0	0	0	33	0	15		
219	1	30	60	10	0	0	0	0	0	10	0	0		

5

10

15

20

TABLE 7

Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance $\Delta C\%$ DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity Log $\rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25 ~ +85°C (%)	$\Delta C/C25\%$ -55 ~ +125°C (%)			
201	1250	1940	2.4	-41	-7.7	-11.2	13.2	14	92
202	1250	1910	2.3	-42	-7.5	-11.2	13.2	15	96
203	1250	1950	2.4	-42	-8.1	-11.6	13.3	14	88
204	1250	1920	2.3	-44	-7.8	-11.5	13.2	15	85
205	1250	1930	2.3	-41	-8.1	-11.5	13.2	14	91
206	1250	1890	2.2	-40	-8.0	-12.1	13.4	14	95
207	1250	1910	2.3	-43	-8.1	-11.7	13.3	14	88
208	1250	1900	2.3	-42	-8.3	-11.8	13.3	14	92
209	1250	1930	2.3	-43	-8.1	-11.9	13.3	14	88
210	1250	1920	2.3	-43	-8.1	-12.5	13.3	14	85
211	1250	1880	2.2	-41	-7.5	-11.1	13.5	15	96
212	1250	1920	2.3	-42	-8.3	-11.8	13.6	14	92
213	1300	1620	3.1	-42	-7.2	-12.1	11.2	8	-
214	1300	1530	2.9	-42	-7.3	-11.8	11.1	8	-
215	1300	1460	2.7	-40	-7.2	-12.5	11.4	9	-
216	1300	1470	2.7	-40	-7.8	-12.9	11.3	9	-
217	1300	1430	2.9	-38	-7.1	-11.7	11.5	8	-
218	1300	1510	2.8	-41	-6.6	-11.2	11.4	8	-
219	1300	1480	3.1	-40	-7.1	-12.2	11.2	8	-

As are evident from Table 6 and Table 7, the sample Nos. 201 to 210 in which  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxides with compositions within the area surrounded by the straight lines connecting between the succeeding two points represented by A ( $x = 85$ ,  $y = 1$ ,  $z = 14$ ), B ( $x = 35$ ,  $y = 51$ ,  $z = 14$ ), C ( $x = 30$ ,  $y = 20$ ,  $z = 50$ ) and D ( $x = 39$ ,  $y = 1$ ,  $z = 60$ ) or on the lines in a ternary composition diagram having apexes represented by each component  $\text{SiO}_2$ ,  $\text{TiO}_2$  and XO ( $x$ ,  $y$  and  $z$  are represented by mol%) are added, has a dielectric constant of as large as 1890 or more, the rate of temperature dependent changes of the electrostatic capacitance satisfy the B-grade characteristic standard prescribed in the JIS standard in the temperature range from  $-25^\circ\text{C}$  to  $+85^\circ\text{C}$ , and satisfy the X7R-grade characteristic standard prescribed in the EIA standard in the temperature range from  $-55^\circ\text{C}$  to  $+125^\circ\text{C}$ . In addition, the rate of change of the capacitance when a DC voltage of 5 kV/mm is impressed is as small as within 44%, the change of the electrostatic capacitance being small when used as thin layers. The mean lifetime under the high temperature load test is as long as 85 hours or more, enabling a firing temperature of  $1250^\circ\text{C}$ .

When the compositions of the  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxides are out of the range of the present invention as in the sample Nos. 213 to 216 and 219, on the contrary, sintering is insufficient, immediately causing short circuit troubles when a voltage is impressed in the high temperature load test.

While the resistivity can be enhanced by allowing  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  in the  $\text{SiO}_2$ - $\text{TiO}_2$ -XO based oxides as in the sample Nos. 211 and 212, sintering becomes insufficient when the amount of addition of  $\text{Al}_2\text{O}_3$  exceeds

about 15 parts by weight or the amount of addition of  
ZrO<sub>2</sub> exceeds about 5 parts by weight as in the sample  
Nos. 217 and 218, immediately causing short circuit  
troubles when a voltage is impressed in the high  
5 temperature load test.

When the dielectric ceramic particles of the  
samples having the compositions within the range of the  
present invention obtained in the Examples 1 to 3 were  
analyzed with a transmission electron microscope, core-  
10 shell structures in which the Re components (Re denotes  
Y, Gd, Tb, Dy, Ho, Er and Yb) are diffused in the  
vicinity of and at the grain boundary were confirmed.

As is evident from the foregoing descriptions,  
the dielectric ceramic layers in the laminated ceramic  
15 capacitor according to the present invention are composed  
of a dielectric ceramic composition that is not reduced  
even when they are fired in a reducing atmosphere.  
Therefore, base metals such as nickel and a nickel alloy  
can be used as electrode materials, along with making it  
20 possible to reduce the production cost of the laminated  
ceramic capacitor because the material is able to be  
fired at a relatively low temperature of 1250°C.

Reduction of the dielectric constant, or the  
electrostatic capacitance, is small even when a high  
25 electric field is impressed on the thin layer of the  
dielectric ceramic layer in the laminated ceramic  
capacitor using the dielectric ceramic composition,  
ensuring high reliability enough for obtaining a small  
size and thin layered laminated ceramic capacitor having  
30 large capacitance.

The dielectric ceramic layers 2a and 2b may be  
composed of a dielectric ceramic composition containing  
the principal components comprising barium calcium

652020-00099  
titanate  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$ , at least one or more of the  
oxides selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$   
and  $\text{Yb}_2\text{O}_3$ ,  $\text{MgO}$  and  $\text{MnO}$ ; and a sub-component selected from  
5  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si}, \text{Ti})\text{O}_2$  based oxides,  $\text{Al}_2\text{O}_3-\text{MO}-\text{B}_2\text{O}_3$  based oxides  
(MO is at least one oxide selected from  $\text{BaO}$ ,  $\text{CaO}$ ,  $\text{SrO}$ ,  
 $\text{MgO}$ ,  $\text{ZnO}$  and  $\text{MnO}$ ) and  $\text{SiO}_2$ . The composition described  
above allows the ceramic composition to be fired in a  
reducing atmosphere without endowing it with  
semiconductive properties. Consequently, a highly  
10 reliable laminated ceramic capacitor with high insulation  
resistance at room temperature and at high temperatures  
and having excellent insulation strength can be obtained  
while the temperature characteristics of the  
electrostatic capacitance satisfying the B-grade  
15 characteristics prescribed in the JIS standard and X7R-  
grade characteristics prescribed in the EIA standard.

A highly reliable ceramic capacitor, in which  
the electric field dependent change of dielectric  
constant is small even when thin ceramic layers are  
20 placed in a high field intensity, can be obtained by  
using a barium calcium titanate material with a mean  
particle size of about 0.1 to 0.7  $\mu\text{m}$ . The dielectric  
ceramic has a core-shell structure in which Re components  
(Re is one or more of the elements selected from Y, Gd,  
25 Tb, Dy, Ho, Er and Yb) are distributed in the vicinity  
and at the grain boundaries due to diffusion during  
firing.

A highly reliable dielectric material is also  
obtainable by using a barium calcium titanate material  
30 containing about 0.02% by weight or less of alkali metal  
oxides such as  $\text{Na}_2\text{O}$  and  $\text{K}_2\text{O}$ .

Although the ratio (n) of (barium +  
calcium)/titanium in the barium calcium titanate material

is not especially limited, the ratio (n) in the range from about 0.990 to 1.035 is desirable in order to diminish particle size distribution in the synthesized powder when stability for producing the powder material is taken into consideration.

The  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si},\text{Ti})\text{O}_2$  based oxides contained in the principal component allows the ceramic to be sintered at a relatively low temperature of  $1250^\circ\text{C}$  with no fear of deterioration of its characteristics due to plating. A much higher insulation resistance is obtained by allowing  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  to be contained in the  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si}, \text{Ti})\text{O}_2$  based oxides. The  $\text{Al}_2\text{O}_3-\text{MO}-\text{B}_2\text{O}_3$  based oxides contained in the principal component allows the ceramic to be easily sintered with no fear of deterioration of its characteristics due to plating. Further,  $\text{SiO}_2$  contained in the principal component also allows the ceramic to be easily sintered with no fear of deterioration of its characteristics due to plating.

The inner electrodes are composed of a base metal such as nickel and a nickel alloy.

The outer electrodes are composed of a sintered layer comprising various conductive metals such as Ag, Pd, Ag-Pd, Cu and a Cu alloy, or a sintered layer produced by blending the conductive metal powder with  $\text{B}_2\text{O}_3-\text{LiO}_2-\text{SiO}_2-\text{BaO}$  based,  $\text{B}_2\text{O}_3-\text{SiO}_2-\text{BaO}$  based,  $\text{LiO}_2-\text{SiO}_2-\text{BaO}$  based or  $\text{B}_2\text{O}_3-\text{SiO}_2-\text{ZnO}$  based glass frits. Plating layers can be formed on this sintered layer. The plating layer may be merely composed of the first plating layer comprising Ni, Cu or a Ni-Cu alloy, or a second plating layer 7 with a solder or tin may be formed thereon.

The foregoing method for producing the laminated ceramic capacitor can be also used when the materials described above are used.



Example 4

TiO<sub>2</sub>, BaCO<sub>3</sub> and CaCO<sub>3</sub> as starting materials were firstly prepared and mixed with crushing. The mixed powder was heated at 1000°C or more to synthesize nine kinds of barium calcium titanate shown in TABLE 1. Mean particle sizes were determined by observing the material under a scanning electron microscope.

Oxides, carbonates and hydroxides were weighed to be in the composition ratio of 0.25Li<sub>2</sub>O-0.10B<sub>2</sub>O<sub>3</sub>-0.07TiO<sub>2</sub>-0.58SiO<sub>2</sub> (molar ratio) of the first sub-component, and a powder was obtained by crushing with mixing. Likewise, oxides, carbonates and hydroxides were weighed to be in the composition ratio of 0.25Al<sub>2</sub>O<sub>3</sub>-0.17BaO-0.03MnO-0.55B<sub>2</sub>O<sub>3</sub> (molar ratio) of the second sub-component, and a powder was obtained by crushing with mixing. The powders of these first and second sub-components were independently placed in crucibles to heat at 1400°C. Respective oxide powders with a mean particle size of 1 μm or less were obtained by quenching followed by crushing.

BaCO<sub>3</sub> or TiO<sub>2</sub>, and Y<sub>2</sub>O<sub>3</sub>, Gd<sub>2</sub>O<sub>3</sub>, Tb<sub>2</sub>O<sub>3</sub>, Dy<sub>2</sub>O<sub>3</sub>, Ho<sub>2</sub>O<sub>3</sub>, Er<sub>2</sub>O<sub>3</sub>, Yb<sub>2</sub>O<sub>3</sub>, MgO and MnO with purity of 99% or more were prepared for adjusting the molar ratio (m) of (Ba, Ca)/Ti in barium calcium titanate. These powder materials, and the oxide powders as the first and second sub-components were weighed to be the compositions shown in TABLE 8. The first and second sub-components were added in parts by weight relative to 100 parts by weight of the principal component (Ba<sub>1-x</sub>Ca<sub>x</sub>O)<sub>m</sub>TiO<sub>2</sub> + αRe<sub>2</sub>O<sub>3</sub> + βMgO + γMnO. A polybutyral based binder and an organic solvent such as ethanol were added into the weighed mixture, which was wet-milled to prepare a ceramic slurry. This ceramic

5

TABLE 8														
Sample No.	Kind of Barium Calcium Titanate	x	m	(Ba <sub>1-x</sub> CaxO) <sub>m</sub> •TiO <sub>2</sub> +αRe <sub>2</sub> O <sub>3</sub> +βMgO+γMnO							β	γ	First Sub-Component (parts by weight)	Second Sub-Component (parts by weight)
				α										
				Y <sub>2</sub> O <sub>3</sub>	Gd <sub>2</sub> O <sub>3</sub>	Tb <sub>2</sub> O <sub>3</sub>	Dy <sub>2</sub> O <sub>3</sub>	Ho <sub>2</sub> O <sub>3</sub>	Er <sub>2</sub> O <sub>3</sub>	Yb <sub>2</sub> O <sub>3</sub>				
1001*	A	0.003	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1002*	D	0.250	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1003*	B	0.100	1.01	0	0	0	0.0005	0	0	0	0.02	0.005	1	0
1004*	B	0.100	1.01	0	0	0	0.11	0	0	0	0.02	0.005	1	0
1005*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.008	0.005	1	0
1006*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.13	0.005	1	0
1007*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.0008	1	0
1008*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.13	1	0
1009*	B	0.100	0.995	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1010*	B	0.100	1	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1011*	B	0.100	1.036	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1012*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	0	0
1013*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.1	0	0
1014*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	5.5	0
1015*	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	0	5.5
1016*	E	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1017	H	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1018	I	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1	0
1019	G	0.100	1.025	0.025	0	0	0	0	0	0	0.02	0.005	0	1
1020	G	0.100	1.02	0	0.08	0	0	0	0	0	0.05	0.008	4	0

TABLE 8 - Cont'd

TABLE 8 - Cont'd														
Sample No.	Kind of Barium Calcium Titanate	x	m	(Ba <sub>1-x</sub> CaxO) <sub>m</sub> •TiO <sub>2</sub> + αRe <sub>2</sub> O <sub>3</sub> + βMgO + γMnO							First Sub-Component (parts by weight)	Second Sub-Component (parts by weight)		
				α									β	γ
				Y <sub>2</sub> O <sub>3</sub>	Gd <sub>2</sub> O <sub>3</sub>	Tb <sub>2</sub> O <sub>3</sub>	Dy <sub>2</sub> O <sub>3</sub>	Ho <sub>2</sub> O <sub>3</sub>	Er <sub>2</sub> O <sub>3</sub>	Yb <sub>2</sub> O <sub>3</sub>				
1021	G	0.100	1.015	0	0	0.05	0	0	0	0	0.05	0.005	3	0
1022	B	0.100	1.01	0	0	0	0	0.02	0	0	0.02	0.05	2	0
1023	B	0.100	1.01	0	0	0	0	0	0	0.02	0.02	0.05	0	1
1024	C	0.200	1.005	0	0	0	0	0	0	0.03	0.02	0.05	0	1
1025	C	0.200	1.005	0.005	0	0	0.02	0	0	0	0.02	0.005	0	1
1026	F	0.080	1.015	0.005	0.015	0	0	0	0	0	0.02	0.005	2	0
1027	F	0.080	1.015	0	0	0	0.02	0	0	0	0.02	0.005	0	2

\* The Samples marked by (\*) are out of the range of the present invention.

Next, a plurality of ceramic green sheets on which the conductive paste layers had been formed were laminated to obtain a laminated body so that the sides where the conductive paste layers are alternately exposed come to the opposite ends. The laminated body was heated at a temperature of 350°C in a N<sub>2</sub> atmosphere. After driving out the binder, the laminated body was fired in a reducing atmosphere comprising a H<sub>2</sub>-N<sub>2</sub>-H<sub>2</sub>O gas with an oxygen partial pressure of 10<sup>-9</sup> to 10<sup>-12</sup> MPa to obtain a ceramic sintered body.

After firing, an Ag paste containing a B<sub>2</sub>O<sub>3</sub>-Li<sub>2</sub>O-SiO<sub>2</sub>-BaO based glass frit was coated on both side faces of the ceramic sintered body, which was baked at a temperature of 600°C in the N<sub>2</sub> atmosphere to form the outer electrodes electrically connected to the inner electrodes.

A plating solution comprising nickel sulfate, nickel chloride and boric acid was prepared, and nickel plating layers were formed on the silver outer electrodes by a barrel plating method. Then, a solder plating solution comprising an AS (alkano-sulfonic acid) bath was prepared and a solder plating was applied on the nickel plating layer by the barrel plating method, obtaining a laminated ceramic capacitor in which the outer electrodes were covered with plating layers.

The laminated ceramic capacitor obtained as described above had an overall dimension with a width of 5.0 mm, a length of 5.7 mm and a thickness of 2.4 mm, the thickness of the effective dielectric ceramic layer inserted between the inner electrodes being 3 μm. The total number of the effective dielectric ceramic layers was five with an area of the confronting electrode per layer of 16.3 × 10<sup>-6</sup> m<sup>2</sup>.

5       The electric characteristics of these laminated ceramic capacitors were then determined. The methods for measuring the electrostatic capacitance, dielectric loss ( $\tan \delta$ ), insulation resistance, DC bias characteristics and temperature dependency (rate of change) of the electrostatic capacitance, the content of the high temperature load test, and the method for measuring dielectric breakdown voltage were the same as hitherto described. The results are listed in TABLE 9.

00413468.W51

TABLE 9

Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance $\Delta C\%$ DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity $\log \rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25 ~ +85°C (%)	$\Delta C/C25\%$ -55 ~ +125°C (%)			
*1001	1300	3310	3.8	-66	-9.5	-15.6	13.1	14	3
*1002	1250	1090	9.5	-33	-4.3	-6.1	13.1	15	26
*1003	1250	2540	5.1	-57	-3.3	-9.7	13.2	14	1
*1004	1250	1200	3.6	-41	-18.4	-23.4	13.3	15	21
*1005	1250	2470	3.3	-59	-14.8	-22.9	12.6	14	74
*1006	1350	1570	3.7	-41	-6.7	-14.2	13.1	14	3
*1007	1250	1890	2.8	-44	-9.4	-14.8	11.7	13	3
*1008	1250	1830	2.7	-41	9.5	-14.7	12.1	14	5
*1009	1250	2070	3.9	-55	-12.4	-19.6	11.4	9	-
*1010	1250	2050	4.7	-58	-12.7	-18.4	11.5	9	-
*1011	1300	1950	4.4	-51	-9.3	-14.7	12.2	10	1
*1012	1350	1610	5.3	-47	-9.2	-14.1	11.5	11	-
*1013	1350	1630	5.2	-48	-9.3	-14.5	11.7	12	1
*1014	1200	1570	3.5	-47	-13.8	-29.5	13.2	14	7
*1015	1200	1680	3.3	-45	-13.5	-27.7	13.1	14	5
*1016	1250	1750	3.7	-45	-10.8	-15.4	13.1	14	18
1017	1250	2470	3.4	-52	-5.1	-7.7	13.2	14	54
1018	1150	1050	2.3	-31	-7.7	-14.3	13.4	14	162
1019	1175	1450	2.4	-33	-9.7	-14.7	13.2	14	108

TABLE 9 - Cont'd

Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance $\Delta C\%$ DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity $\log \rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25 ~ +85°C (%)	$\Delta C/C25\%$ -55 ~ +125°C (%)			
1020	1150	1260	2.3	-31	-9.4	-14.3	13.3	15	111
1021	1175	1310	2.5	-32	-9.5	-14.8	13.3	14	107
1022	1200	1920	2.5	-41	-8.5	-12.8	13.2	14	83
1023	1250	1990	2.4	-43	-8.5	-12.5	13.3	14	81
1024	1250	1430	2.5	-37	-7.1	-10.2	13.1	14	110
1025	1250	1450	2.5	-35	-6.8	-10.8	13.2	14	120
1026	1175	1160	2.4	-33	-9.7	-14.3	13.2	14	91
1027	1175	1270	2.1	-32	-9.8	-14.7	13.2	14	94

\* The Samples marked by (\*) are out of the range of the present invention.

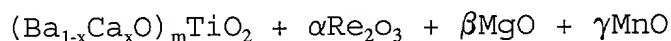


The cross section of the laminated ceramic capacitor was polished and subjected to chemical etching to observe the grain diameter of the dielectric ceramic under a scanning electron microscope. It was found that the grain diameter was almost equal to the particles size of the barium calcium titanate material in the samples having the compositions within the range of the present invention.

As is evident from TABLE 8 and TABLE 9, the rate of temperature dependent changes of the electrostatic capacitance in the laminated ceramic capacitor according to the present invention satisfies the B-grade characteristic standard prescribed in the JIS standard in the temperature range from -25°C to +85°C and the X7R grade characteristic standard prescribed in the EIA standard in the temperature range from -55°C to +125°C. Moreover, the rate of change of the capacitance under an impressed DC voltage of 5 kV/mm is as small as 52%, indicating that the change of the electrostatic capacitance is also small when thin layers are used in the capacitor. The mean lifetime in the high temperature load test is as long as 45 hours, enabling one to fire at a temperature of 1250°C or less.

The reasons why the compositions are limited will be described hereinafter.

In the system comprising the principal component;



( $\text{Re}_2\text{O}_3$  is at least one or more of the compounds selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$ ;  $\alpha$ ,  $\beta$  and  $\gamma$  representing molar ratios), the first and the second sub-components, the content (x) of CaO of about 0.05 or less as in the sample No. 1001 is not preferable since

the rate of impressed voltage dependent change of the capacitance is large and the mean lifetime is extremely shortened. A content ( $x$ ) of CaO exceeding about 0.22 as in the sample No. 1002 is not preferable, on the other

5 hand, since the dielectric loss is increased. Accordingly, the preferable CaO constant ( $x$ ) is in the range of  $0.005 < x \leq 0.22$ .

It is not preferable that the  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) is less than about 0.001 as in the sample No. 1003 since  
10 the mean lifetime is extremely shortened. A  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) of exceeding about 0.10 as in the sample No. 1004 is also not preferable, on the other hand, since the temperature characteristics do not satisfy the B/X7R grade characteristics and the mean lifetime is shortened.  
15 Accordingly, the preferable  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) is in the range of  $0.001 \leq \alpha \leq 0.10$ .

It is not preferable that the MgO content ( $\beta$ ) is less than about 0.001 as in the sample No. 1005 since the temperature characteristics do not satisfy the B/X7R  
20 grade characteristics. A MgO content ( $\beta$ ) of exceeding about 0.12 as in the sample No. 1006 is also not preferable, on the other hand, since the sintering temperature becomes so high that the mean lifetime is extremely shortened. Accordingly, the preferable MgO  
25 content ( $\beta$ ) is in the range of  $0.001 \leq \beta \leq 0.12$ .

It is not preferable that the MnO content ( $\gamma$ ) is about 0.001 or less as in the sample No. 1007 since the resistivity is lowered and the mean lifetime is  
30 extremely shortened. A MnO content ( $\gamma$ ) of exceeding about 0.12 as in the sample No. 1008 is also not preferable, on the other hand, since the mean lifetime is extremely shortened. Accordingly, the preferable MnO content ( $\gamma$ ) is in the range of  $0.001 < \gamma \leq 0.12$ .

It is not preferable that the ratio (m) of (Ba, ca)/Ti is about 1.000 or less as in the sample Nos. 1009 and 1010 since the temperature characteristics do not satisfy the B/X7R grade characteristics and the resistivity becomes low and short circuit troubles are immediately caused when a voltage is impressed in the high temperature load test. It is also not preferable, on the other hand, that the ratio (m) of (Ba, ca)/Ti exceeds about 1.035 as in the sample No. 1011 because sintering becomes insufficient to extremely shorten the mean lifetime. Accordingly, the preferable ratio (m) of (Ba, ca)/Ti is in the range of  $1.000 < m \leq 1.035$ .

It is not preferable that the content of the first and second sub-component is zero as in the sample Nos. 1012 and 1013 since the resistivity becomes low along with immediately causing circuit troubles when a voltage is impressed in the high temperature load test. It is also not preferable, on the other hand, that the content of the first and second sub-components exceed about 5.0 parts by weight as in the sample Nos. 1014 and 1015 because an increased amount of the secondary phase is formed and the temperature characteristics do not satisfy the B/X7R grade characteristics, extremely shortening the mean lifetime. Accordingly, the content of either the first sub-component or the second sub-component is preferably in the range from 0.2 to 5.0.

The content of alkali metal oxides that are contained in barium calcium titanate as impurities is adjusted to about 0.02% by weight or less because, as in the sample No. 1016, the mean lifetime is shortened when the content of the alkali metal oxides exceeds about 0.02% by weight.

The sample No. 1017 in which the mean particle size of barium calcium titanate exceeds  $0.7 \mu\text{m}$  shows a little poor mean lifetime of 52 hours. The sample No. 1018 in which the mean particle size of barium calcium titanate is less than  $0.1 \mu\text{m}$  shows, on the other hand, a little smaller dielectric constant of 1050. Accordingly, the preferable mean particle size of barium calcium titanate is in the range from about  $0.1$  to  $0.7 \mu\text{m}$ .

#### Example 5

Starting materials  $\text{TiO}_2$ ,  $\text{BaCO}_3$  and  $\text{CaCO}_3$  were firstly prepared and mixed with crushing as in Example 4. The mixed powder was heated at  $1000^\circ\text{C}$  or more to synthesize nine kinds of barium calcium titanate shown in TABLE 1. Mean particle sizes were determined by observing the material under a scanning electron microscope.  $\text{SiO}_2$  was also prepared as a third sub-component.

$\text{BaCO}_3$  or  $\text{TiO}_2$  for adjusting the molar ratio (m) of (Ba, Ca)/Ti, and  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$ ,  $\text{Yb}_2\text{O}_3$ ,  $\text{MgO}$  and  $\text{MnO}$  with purity of 99% or more were prepared. These powder materials and the  $\text{SiO}_2$  powder as the third sub-component were weighed to be the compositions shown in TABLE 10. The amount of addition of  $\text{SiO}_2$  is expressed in parts by weight relative to 100 parts by weight of the principal component  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2 + \alpha\text{Re}_2\text{O}_3 + \beta\text{MgO} + \gamma\text{MnO}$ .

TABLE 10													
Sample No.	$(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m \bullet \text{TiO}_2 + \alpha \text{Re}_2\text{O}_3 + \beta \text{MgO} + \gamma \text{MnO}$											Third Sub-Component $\text{SiO}_2$ (parts by weight)	
	Kind of Barium Calcium Titanate	x	m	$\alpha$							$\beta$		$\gamma$
				$\text{Y}_2\text{O}_3$	$\text{Gd}_2\text{O}_3$	$\text{Tb}_2\text{O}_3$	$\text{Dy}_2\text{O}_3$	$\text{Ho}_2\text{O}_3$	$\text{Er}_2\text{O}_3$	$\text{Yb}_2\text{O}_3$			
*1101	A	0.003	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1
*1102	D	0.250	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1
*1103	B	0.100	1.01	0	0	0	0.0005	0	0	0	0.02	0.005	1
*1104	B	0.100	1.01	0	0	0	0.11	0	0	0	0.02	0.005	1
*1105	B	0.100	1.01	0	0	0	0.02	0	0	0	0.0008	0.005	1
*1106	B	0.100	1.01	0	0	0	0.02	0	0	0	0.13	0.005	1
*1107	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.0008	1
*1108	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.13	1
*1109	B	0.100	0.995	0	0	0	0.02	0	0	0	0.02	0.005	1
*1110	B	0.100	1	0	0	0	0.02	0	0	0	0.02	0.005	1
*1111	B	0.100	1.036	0	0	0	0.02	0	0	0	0.02	0.005	1
*1112	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	0
*1113	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.1	0
*1114	B	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	5.5
*1115	E	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1
1116	H	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1
1117	I	0.100	1.01	0	0	0	0.02	0	0	0	0.02	0.005	1
1118	G	0.100	1.025	0.025	0	0	0	0	0	0	0.02	0.005	1
1119	G	0.100	1.02	0	0.08	0	0	0	0	0	0.05	0.008	4
1120	G	0.100	1.015	0	0	0.05	0	0	0	0	0.05	0.005	3

TABLE 10 - Cont'd													
Sample No.	Kind of Barium Calcium Titanate	x	m	(Ba <sub>1-x</sub> Ca <sub>x</sub> O) <sub>m</sub> •TiO <sub>2</sub> +αRe <sub>2</sub> O <sub>3</sub> +βMgO+γMnO							β	γ	Third Sub-Component SiO <sub>2</sub> (parts by weight)
				α									
				Y <sub>2</sub> O <sub>3</sub>	Gd <sub>2</sub> O <sub>3</sub>	Tb <sub>2</sub> O <sub>3</sub>	Dy <sub>2</sub> O <sub>3</sub>	Ho <sub>2</sub> O <sub>3</sub>	Er <sub>2</sub> O <sub>3</sub>	Yb <sub>2</sub> O <sub>3</sub>			
1121	B	0.100	1.01	0	0	0	0	0.02	0	0	0.02	0.05	2
1122	B	0.100	1.01	0	0	0	0	0	0.02	0	0.02	0.05	1
1123	C	0.200	1.005	0	0	0	0	0	0	0.03	0.02	0.05	1
1124	C	0.200	1.005	0.005	0	0	0.02	0	0	0	0.02	0.005	1
1125	F	0.080	1.015	0.005	0.015	0	0	0	0	0	0.02	0.005	1
1126	F	0.080	1.015	0	0	0	0.02	0	0	0	0.02	0.005	0.5

\*The samples marked by (\*) are out of the range of the present invention.

Laminated ceramic capacitors were then produced by the same method as in Example 4. The size and shape of the laminated ceramic capacitors produced were the same as those in Example 4. The electric characteristics were measured by the same method as used in Example 1, the results of which are shown in TABLE 11.

5

00413468.W51

TABLE 11

Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance $\Delta C\%$ DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity $\log \rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25 ~ +85°C (%)	$\Delta C/C25\%$ -55 ~ +125°C (%)			
*1101	1300	1340	3.0	-68	-9.8	-15.4	13.1	15	4
*1102	1250	1110	9.4	-33	-4.5	-6.7	13.2	14	21
*1103	1250	2410	2.1	-57	-1.7	-10.6	13.3	14	1
*1104	1250	1250	2.9	-57	-18.2	-13.5	13.5	15	11
*1105	1250	2610	2.5	-65	-15.5	-25.1	11.5	11	13
*1106	1350	1820	2.7	-48	-7.9	-15.1	13.1	15	1
*1107	1250	1910	2.2	-56	-9.2	-15.3	11.2	14	14
*1108	1250	1700	2.4	-54	-14.1	-20.1	11.4	14	7
*1109	1250	2050	4.5	-59	-12.3	-19.2	11.2	9	-
*1110	1250	1980	2.8	-63	-12.5	-17.2	11.7	8	-
*1111	1300	2070	3.1	-52	-9.0	-14.1	12.4	8	2
*1112	1350	1530	3.5	-44	-8.7	-13.5	11.1	11	-
*1113	1350	1510	3.9	-47	-8.7	14.0	11.3	8	-
*1114	1200	1720	2.8	-49	-15.2	-29.8	13.2	14	4
*1115	1250	1710	2.2	-59	-15.1	-16.5	13.1	14	10
1116	1250	2900	1.7	-52	-4.8	-6.5	13.2	13	62
1117	1150	1130	2.1	-31	-10.2	-14.9	13.3	15	190
1118	1175	1400	2.1	-34	-9.4	-14.2	13.4	15	89
1119	1150	1270	2.4	-34	-8.7	-14.1	13.2	14	109



TABLE 11 - Cont'd

Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance AC% DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity Log $\rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25 ~ +85°C (%)	$\Delta C/C25\%$ -55 ~ +125°C (%)			
1120	1175	1270	2.3	-35	-9.3	-14.3	13.1	14	100
1121	1200	1910	2.0	-43	-8.8	-13.5	13	15	84
1122	1250	2030	2.1	-41	-7.9	-13.2	13.3	14	92
1123	1250	1410	2.3	-35	-8.1	-11.8	13.1	14	115
1124	1250	1420	2.4	-30	-7.9	-11.0	13	14	132
1125	1175	1270	2.1	-33	-9.8	-14.3	13.2	15	89
1126	1175	1310	2.0	-31	-9.2	-13.7	13.2	15	98

\* The samples marked by (\*) are out of the range of the present invention.

5 The grain size of the polished cross section of the laminated ceramic capacitor obtained was determined under a scanning electron microscope after chemical etching, finding that the grain size was almost equal to the particle size of the barium calcium titanate as a starting material in the samples having the compositions within the range of the present invention.

10 As is evident from TABLE 10 and TABLE 11, the rate of temperature dependent change of the laminated ceramic capacitor according to the present invention satisfies the B-grade characteristic standard prescribed in the JIS standard in the temperature range from -15°C to +85°C and the X7R-grade characteristic standard prescribed in the EIA standard in the temperature range  
15 from -55°C to +125°C. Moreover, the rate of change of the capacitance under an impressed DC voltage of 5 kV/mm is as small as 52%, indicating that the change of the electrostatic capacitance is also small when the capacitor is used as a thin layer. The mean lifetime in  
20 the high temperature load test is as long as 62 hours, enabling one to fire at a temperature of 1250°C or less.

The reason why the compositions according to the present invention are limited in the present invention will be described hereinafter.

25 In the system comprising the principal component

$$(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2 + \alpha\text{Re}_2\text{O}_3 + \beta\text{MgO} + \gamma\text{MnO}$$
  
30  $(\text{Re}_2\text{O}_3$  represents at least one of the compounds selected from  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$  and  $\alpha$ ,  $\beta$  and  $\gamma$  represent molar ratios) and the third sub-component, a content (x) of CaO of about 0.005 or less as in the sample No. 1101 is not preferable since the rate of impressed voltage dependent change of the capacitance

becomes large besides the mean lifetime becomes extremely short. It is also not preferable that the content (x) of CaO exceeds about 0.22 as in the sample No. 1102 because the dielectric loss is increased. Accordingly, the preferable CaO content (x) is in the range of  $0.005 < x \leq 0.22$ .

A  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) of less than about 0.001 as in the sample No. 1103 is also not preferable because the mean lifetime becomes extremely short. It is also not preferable that the content of  $\text{Re}_2\text{O}_3$  ( $\alpha$ ) exceeds about 0.10 as in the sample No. 1104 since the temperature characteristics do not satisfy the B/X7R-grade characteristics while the mean lifetime is shortened. Accordingly, the preferable  $\text{Re}_2\text{O}_3$  content ( $\alpha$ ) is in the range of  $0.001 \leq \alpha \leq 0.10$ .

A MgO content ( $\beta$ ) of less than about 0.001 as in the sample No. 1105 is also not preferable because the rate of impressed voltage dependent change of the capacitance becomes large, the temperature characteristics do not satisfy the B/X7R-grade characteristics and the resistivity is lowered, shortening the mean lifetime. It is also not preferable, on the other hand, that the amount of addition ( $\beta$ ) of MgO exceeds about 0.12 as in the sample No. 1106 since the sintering temperature becomes high to extremely shorten the mean lifetime. Accordingly, the preferable MgO content ( $\beta$ ) is in the range of  $0.001 \leq \beta \leq 0.12$ .

A MnO content ( $\gamma$ ) of less than about 0.001 as in the sample No. 1107 is also not preferable because the resistivity is low while the mean lifetime is shortened. It is also not preferable, on the other hand, that the MnO content ( $\gamma$ ) exceeds about 0.12 as in the sample No. 1108 since the temperature characteristics do not satisfy

the B/X7R-grade characteristics, the resistivity becomes low and the mean lifetime is shortened. Accordingly, the preferable range of the MnO content ( $\gamma$ ) is  $0.001 \leq \gamma \leq 0.12$ .

5                   It is not preferable that the ratio (m) of (Ca, Ca)/Ti is less than about 1.000 as in the sample Nos. 1109 and No. 1110 because the temperature characteristics do not satisfy the B/X7R-grade characteristics and the resistivity is lowered, immediately causing short circuit troubles when a voltage is impressed in the high  
10                   temperature load test. It is also not preferable, on the other hand, that the ratio (m) of (Ca, Ca)/Ti exceed about 1.035 as in the sample No. 1111 because sintering is insufficient to extremely shorten the mean lifetime.  
15                   Accordingly, the preferable ratio (m) of (Ca, Ca)/Ti is in the range of  $1.000 < m \leq 1.035$ .

                  It is not preferable that the contents of the first and second sub-components are zero as in the samples No. 1112 and No. 1113 because the resistivity is  
20                   lowered to immediately cause short circuit troubles when a voltage is impressed in the high temperature load test. It is also not preferable, on the other hand, that the contents of the first and second sub-components exceed about 5.0 parts by weight as in the sample No. 1114  
25                   because the second phase based on glass components is increased besides the temperature characteristics do not satisfy the B/X7R-grade characteristics and the mean lifetime is extremely shortened. Accordingly, the preferable content of either the first component or the  
30                   second component is in the range from about 0.2 to 5.0 parts by weight.

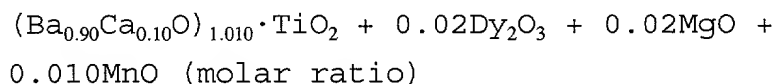
                  The content of the alkali metal oxides contained in barium calcium titanate as impurities is

adjusted to about 0.02% by weight or less because when the content of the alkali metal oxides exceeds about 0.02% by weight as in the sample No. 1115, the mean lifetime is shortened.

5                   The sample No. 1116 in which the mean particle size of barium calcium titanate exceeds about 0.7  $\mu\text{m}$  shows a little poor mean lifetime of 52 hours. The sample No. 1117 in which the mean particle size of barium calcium titanate is less than about 0.1  $\mu\text{m}$  shows, on the  
10                   other hand, a little smaller dielectric constant of 1130. Accordingly, the preferable mean particle size of barium calcium titanate is in the range from 0.1 to 0.7  $\mu\text{m}$ .

#### Example 6

15                   A starting material having the following composition was prepared as a dielectric powder using barium calcium titanate (B) as shown in TABLE 12:



20                   Laminated ceramic capacitors were produced by the same method as used in Example 1, except that the  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si}, \text{Ti})\text{O}_2$  based oxide (including those supplemented with  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$ ) as the first sub-component with a mean particle size of 1  $\mu\text{m}$  or less produced by heating at 1200 to 1500°C was added to the  
25                   powder material. The size and shape of the laminated ceramic capacitor produced are the same as that produced in Example 4. The electric characteristics were measured by the same method as in Example 4, the results of which are shown in TABLE 13.

TABLE 12							
Sample. No.	First Subcomponent					Additive	
	Amount of addition (parts by weight)	Composition (mol%, except w)				Parts by Weight	
		Li <sub>2</sub> O	B <sub>2</sub> O <sub>3</sub>	(Si <sub>w</sub> Ti <sub>1-w</sub> )	w	Al <sub>2</sub> O <sub>3</sub>	ZrO <sub>2</sub>
1201	1	0	20	80	0.7	0	0
1202	1	19	1	80	0.7	0	0
1203	1	49	1	50	0.8	0	0
1204	2	45	50	5	0.5	0	0
1205	2	20	75	5	0.4	0	0
1206	2	0	80	20	0.4	0	0
1207	1.5	35	15	50	0.5	0	0
1208	1.5	35	50	15	0.9	0	0
1209	2	20	40	40	0.3	0	0
1210	2	10	15	75	0.7	0	0
1211	2	10	70	20	0.4	5	2
1212	2	35	15	50	0.7	15	5
1213	2	35	15	50	0.7	20	0
1214	2	35	15	50	0.7	0	10
1215	3	10	5	85	0.5	0	0
1216	3	55	20	25	0.7	0	0
1217	3	35	62	3	0.7	0	0
1218	2	5	85	10	0.7	0	0
1219	2	10	15	75	0.1	0	0
1220	2	35	50	15	1	0	0
1221	2	35	50	15	0.7	30	0
1222	1	35	50	15	0.7	0	20

TABLE 13

Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance $\Delta C\%$ DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity $\log \rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25 ~ +85°C (%)	$\Delta C/C25\%$ -55 ~ +125°C (%)			
1201	1250	1880	2.4	-42	-7.8	-12.5	13.0	13	81
1202	1250	1870	2.4	-43	-7.6	-12.4	13.1	13	88
1203	1250	1850	2.3	-42	-7.8	-12.4	13.1	13	83
1204	1225	1830	2.3	-41	-7.7	-12.1	13.1	13	85
1205	1225	1860	2.5	-41	-7.1	-12.1	13.0	13	84
1206	1225	1840	2.4	-40	-8.1	-12.5	13.1	13	80
1207	1250	1880	2.4	-43	-8.0	-11.8	13.0	13	86
1208	1250	1900	2.5	-45	-8.3	-12.7	13.0	12	88
1209	1225	1850	2.4	-44	-7.7	-12.3	13.1	13	83
1210	1225	1870	2.4	-45	-7.9	-12.5	13.0	13	83
1211	1225	1880	2.4	-44	-8.0	-12.6	13.3	14	91
1212	1225	1860	2.3	-44	-8.5	-12.5	13.3	14	97
1213	1225	1810	2.2	-43	-8.2	-12.4	13.4	14	95
1214	1225	1780	2.2	-43	-7.5	-12.1	13.3	14	92
1215	1350	1650	4.3	-42	-7.2	-11.7	11.1	12	2
1216	1350	1770	4.1	-42	-7.4	-11.8	11.4	10	7
1217	1300	1580	3.5	-41	-7.3	-11.3	11.6	11	26
1218	1300	1870	3.4	-44	-7.8	-11.8	11.8	11	18
1219	1350	1830	4.7	-44	-7.7	-12.1	11.1	11	4

5

10

15

20





As is evident from TABLE 12 and TABLE 13, the sample Nos. 1201 to 1210, in which  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$  based oxides with compositions within the area surrounded by the straight lines connecting between the succeeding two points represented by A ( $x = 0, y = 20, z = 80$ ), B ( $x = 19, y = 1, z = 80$ ), C ( $x = 49, y = 1, z = 50$ ), D ( $x = 45, y = 50, z = 5$ ), E ( $x = 20, y = 75, z = 5$ ) and F ( $x = 0, y = 80, z = 20$ ) or on the lines in a ternary composition diagram having apexes represented by each component  $\text{Li}_2\text{O}$ ,  $\text{B}_2\text{O}_3$  and  $\text{Si}_w\text{Ti}_{1-w})\text{O}_2$  ( $x, y$  and  $z$  are represented by mol%) are added, has a dielectric constant of as large as 1830 or more, the rate of temperature dependent changes of the electrostatic capacitance satisfy the B-grade characteristic standard prescribed in the JIS standard in the temperature range from  $-25^\circ\text{C}$  to  $+85^\circ\text{C}$ , and satisfy the X7R-grade characteristic standard prescribed in the EIA standard in the temperature range from  $-55^\circ\text{C}$  to  $+125^\circ\text{C}$ . In addition, the rate of change of the capacitance when a DC voltage of 5 kV/mm is impressed is as small as within 45%, the change of the electrostatic capacitance being small when used as thin layers. The mean lifetime under the high temperature load test is as long as 80 hours or more, enabling a firing temperature of  $1250^\circ\text{C}$ .

When the content of the  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si}, \text{Ti})\text{O}_2$  based oxide is out of the range of the present invention as in the sample Nos. 1215 and 1220, on the contrary, sintering is insufficient or electric characteristics are deteriorated due to plating after firing, shortening the mean lifetime in the high temperature load test.

While the resistivity can be enhanced by allowing  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  to be contained in the  $\text{Li}_2\text{O}-\text{B}_2\text{O}_3-(\text{Si}, \text{Ti})\text{O}_2$  based oxide as in the sample Nos. 1211 and

1214, sintering becomes insufficient to shorten the mean lifetime in the high temperature load test as in the sample Nos. 1221 and 1222 when the amount of addition of  $\text{Al}_2\text{O}_3$  exceeds 20 parts by weight or the amount of addition of  $\text{ZrO}_2$  exceeds 10 parts by weight.

Example 7

A starting material having the following composition was prepared as a dielectric powder using barium calcium titanate (B) as shown in TABLE 14:

( $\text{Ba}_{0.90}\text{Ca}_{0.10}\text{O}$ )<sub>1.010</sub> ·  $\text{TiO}_2$  + 0.02 $\text{Gd}_2\text{O}_3$  + 0.05 $\text{MgO}$  + 0.010 $\text{MnO}$  (molar ratio)

Laminated ceramic capacitors were produced by the same method as used in Example 1, except that the  $\text{Al}_2\text{O}_3$ - $\text{MO}$ - $\text{B}_2\text{O}_3$  based oxide as the second sub-component with a mean particle size of 1  $\mu\text{m}$  or less produced by heating at 1200 to 1500°C as shown in TABLE 14 was added to the powder material. The size and shape of the laminated ceramic capacitor produced are the same as that produced in Example 4. The electric characteristics were measured by the same method as in Example 4, the results of which are shown in TABLE 15.

TABLE 14										
Sample No.	The Second Sub-Component									
	Amount of Addition	Composition (mol%)								
		Al <sub>2</sub> O <sub>3</sub>	MO							B <sub>2</sub> O <sub>3</sub>
			BaO	CaO	SrO	MgO	ZnO	MnO	Total	
1301	1	1	5	5	0	0	0	4	14	85
1302	1	20	8	0	0	0	2	0	10	70
1303	1	30	6	10	2	2	0	0	20	50
1304	1	40	0	30	0	0	5	15	50	10
1305	1	20	0	30	0	0	10	30	70	10
1306	1	1	0	5	5	24	5	0	39	60
1307	1	15	10	0	0	0	3	2	15	70
1308	1	10	10	15	0	5	0	5	35	55
1309	1	20	0	30	5	0	3	2	40	40
1310	1	30	5	35	5	0	5	0	50	20
1311	1	5	10	0	0	0	0	0	10	85
1312	1	30	5	5	0	0	0	0	10	60
1313	1	40	20	0	0	0	3	2	25	35
1314	1	60	30	0	0	0	3	2	35	5
1315	1	5	15	35	10	0	3	2	65	30
1316	1	0	15	15	0	0	0	0	30	70

TABLE 15									
Sample No.	Burning Temperature (°C)	Dielectric Constant	Dielectric Loss $\tan \delta$ (%)	Rate of Change of Capacitance $\Delta C\%$ DC 5Kv/mm	Rate of Temperature Dependent Change of Capacitance		Resistivity Log $\rho$ ( $\Omega \cdot \text{cm}$ )	Dielectric Breakdown Voltage DC (kV/mm)	Mean Lifetime (h)
					$\Delta C/C20\%$ -25~+85°C (%)	$\Delta C/C25\%$ -55~+125°C (%)			
1301	1250	1860	2.4	-43	-7.2	-10.9	13.2	13	87
1302	1250	1870	2.4	-43	-7.3	-11.1	13.1	13	87
1303	1250	1900	2.5	-45	-8.1	-12.2	13.2	13	84
1304	1250	1880	2.4	-45	-7.8	-12.2	13.2	13	88
1305	1250	1890	2.4	-43	-8.0	-12.3	13.2	13	92
1306	1250	1850	2.3	-43	-7.9	-12.1	13.2	14	88
1307	1250	1870	2.5	-44	-7.5	-11.9	13.2	13	90
1308	1250	1880	2.5	-45	-7.9	-12.2	13.3	13	88
1309	1250	1790	2.3	-43	-7.3	-11.8	13.2	14	92
1310	1250	1830	2.3	-42	-8.0	-12.1	13.2	13	87
1311	1350	1780	3.7	-41	-7.8	-11.8	11.5	11	3
1312	1350	1560	4.5	-41	-7.1	-11.4	10.9	10	2
1313	1350	1630	5.1	-43	-7.8	-11.7	11.1	10	1
1314	1350	1810	3.5	-48	-8.4	-12.1	11.2	11	2
1315	1350	1650	5.7	-44	-7.7	-11.9	11.1	11	4
1316	1250	1820	4.8	-47	-8.1	-12.5	11.4	12	5

5

10

15

As is evident from TABLE 14 and TABLE 15, the sample Nos. 1301 to 1310, in which  $\text{Al}_2\text{O}_3$ -MO- $\text{B}_2\text{O}_3$  based oxides with compositions within the area surrounded by the straight lines connecting between the succeeding two points represented by A ( $x = 1$ ,  $y = 14$ ,  $z = 85$ ), B ( $x = 20$ ,  $y = 10$ ,  $z = 70$ ), C ( $x = 30$ ,  $y = 20$ ,  $z = 50$ ), D ( $x = 40$ ,  $y = 50$ ,  $z = 10$ ), E ( $x = 20$ ,  $y = 70$ ,  $z = 10$ ) and F ( $x = 1$ ,  $y = 39$ ,  $z = 60$ ) or on the lines in a ternary composition diagram having apexes represented by each component  $\text{Al}_2\text{O}_3$ , MO and  $\text{B}_2\text{O}_3$  are added, have a dielectric constant of as large as 1790 or more, the rate of temperature dependent changes of the electrostatic capacitance satisfy the B-grade characteristic standard prescribed in the JIS standard in the temperature range from  $-25^\circ\text{C}$  to  $+85^\circ\text{C}$ , and satisfy the X7R-grade characteristic standard prescribed in the EIA standard in the temperature range from  $-55^\circ\text{C}$  to  $+125^\circ\text{C}$ . In addition, the rate of change of the capacitance when a DC voltage of 5 kV/mm is impressed is as small as within 45%, the change of the electrostatic capacitance being small when used as thin layers. The mean lifetime under the high temperature load test is as long as 84 hours or more, enabling a firing temperature of  $1250^\circ\text{C}$ .

When the content of the  $\text{Al}_2\text{O}_3$ -MO- $\text{B}_2\text{O}_3$  based oxide is out of the range of the present invention as in the sample Nos. 1311 to 1316, on the contrary, sintering is insufficient or electric characteristics are deteriorated due to plating after firing, shortening the mean lifetime in the high temperature load test.

From the results obtained by analyzing the in the dielectric ceramic particles under a transmission electron microscope with respect to the samples having the compositions within the range of the present

invention obtained in Examples 4 to 7, it was confirmed that all the samples have core-shell structures in which the Re components (Re represents Y, Gd, Tb, Dy, Ho, Er and Yb) are diffused in the vicinity of or at the grain boundaries.

Accordingly, the present invention provides a highly reliable and plating solution resistive ceramic capacitor using Ni or a Ni alloy for the inner electrodes.

09363939-090699

WHAT IS CLAIMED IS:

1. A dielectric ceramic comprising  
(Ba<sub>1-x</sub>Ca<sub>x</sub>O)<sub>m</sub>TiO<sub>2</sub> + αRe<sub>2</sub>O<sub>3</sub> + βMgO + γMnO  
in which Re is at least one member selected from the  
group consisting of Y, Gd, Tb, Dy, Ho, Er and Yb; α, β γ,  
5 m and x are molar ratios; 0.001 ≤ α ≤ 0.10; 0.001 ≤ β ≤  
0.12; 0.001 < γ ≤ 0.12; 1.000 < m ≤ 1.035; and 0.005 < x  
≤ 0.22, and

about 0.2 to 5.0 parts by weight of either  
a first sub-component or a second sub-component or a  
10 third sub-component relative to 100 parts by weight of  
(Ba<sub>1-x</sub>Ca<sub>x</sub>O)<sub>m</sub>TiO<sub>2</sub>, wherein

the (Ba<sub>1-x</sub>Ca<sub>x</sub>O)<sub>m</sub>TiO<sub>2</sub> contains about 0.02% by  
weight or less of alkali metal oxides,

the first sub-component is a Li<sub>2</sub>O-(Si,Ti)O<sub>2</sub>-MO  
15 oxide in which M is at least one of Al and Zr,

the second sub-component is a SiO<sub>2</sub>-TiO<sub>2</sub>-XO oxide  
in which X is at least one selected from the group  
consisting of Ba, Ca, Sr, Mg, Zn and Mn, and

the third sub-component is SiO<sub>2</sub>.

2. A dielectric ceramic according to Claim 1,  
wherein the (Ba<sub>1-x</sub>Ca<sub>x</sub>O)<sub>m</sub>TiO<sub>2</sub> has a mean particle size of  
about 0.1 to 0.7 μm.

3. A dielectric ceramic according to Claim 1,  
wherein the first sub-component is present and comprises  
xLiO<sub>2</sub>-y(Si<sub>w</sub>Ti<sub>1-w</sub>)O<sub>2</sub>-zMO, x, y and z are molar percentages  
and 30 ≤ w ≤ 1.0, and is within the area surrounded by  
5 the straight lines connecting between the succeeding two  
points represented by A (x = 20, y = 80, z = 0), B (x =

10,  $y = 80$ ,  $z = 10$ ), C ( $x = 10$ ,  $y = 70$ ,  $z = 20$ ), D ( $x = 35$ ,  $y = 45$ ,  $z = 20$ ), E ( $x = 45$ ,  $y = 45$ ,  $z = 10$ ) and F ( $x = 45$ ,  $y = 55$ ,  $z = 0$ ) or on said lines in a ternary composition diagram having apexes represented by the components  $\text{LiO}_2$ ,  $(\text{Si}_w\text{Ti}_{1-w})\text{O}_2$  and  $\text{MO}$ , provided that when the component is on the line A-F,  $0.3 \leq w < 1.0$ .

4. A dielectric ceramic according to Claim 3, wherein comprising at least one of  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  in a combined amount of about 20 parts by weight or less and in which the  $\text{ZrO}_2$  is 10 parts by weight or less relative to 100 parts by weight of the  $\text{Li}_2\text{O}-(\text{Si},\text{Ti})\text{O}_2$ -MO oxide.

5. A dielectric ceramic according to Claim 3, wherein said points are A ( $x = 0$ ,  $y = 20$ ,  $z = 80$ ), B ( $x = 19$ ,  $y = 1$ ,  $z = 80$ ), C ( $x = 49$ ,  $y = 1$ ,  $z = 50$ ), D ( $x = 45$ ,  $y = 50$ ,  $z = 5$ ), E ( $x = 20$ ,  $y = 75$ ,  $z = 5$ ) and F ( $x = 0$ ,  $y = 80$ ,  $z = 20$ ) and wherein the  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$  has a mean particle size of about 0.1 to 0.7  $\mu\text{m}$ .

6. A dielectric ceramic according to Claim 1, wherein the second sub-component is present and comprises  $x\text{SiO}_2$ - $y\text{TiO}_2$ - $z\text{XO}$ ,  $x$ ,  $y$  and  $z$  are molar percentages, and is within the area surrounded by the straight lines connecting between the succeeding two points represented by A ( $x = 85$ ,  $y = 1$ ,  $z = 14$ ), B ( $x = 35$ ,  $y = 51$ ,  $z = 14$ ), C ( $x = 30$ ,  $y = 20$ ,  $z = 50$ ) and D ( $x = 39$ ,  $y = 1$ ,  $z = 60$ ) or on said lines in a ternary composition diagram having apexes represented by the components  $\text{SiO}_2$ ,  $\text{TiO}_2$  and  $\text{XO}$ .

7. A dielectric ceramic according to Claim 6, comprising at least one of  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$  in a combined



amount of about 15 parts by weight or less and the  $\text{ZrO}_2$  is 5 parts by weight or less relative to 100 parts by weight of the  $\text{SiO}_2\text{-TiO}_2\text{-XO}$  oxide.

8. A dielectric ceramic according to Claim 6, wherein said points are A ( $x = 1$ ,  $y = 14$ ,  $z = 85$ ), B ( $x = 20$ ,  $y = 10$ ,  $z = 70$ ), C ( $x = 30$ ,  $y = 20$ ,  $z = 50$ ), D ( $x = 40$ ,  $y = 50$ ,  $z = 10$ ), E ( $x = 20$ ,  $y = 70$ ,  $z = 10$ ) and F ( $x = 1$ ,  $y = 39$ ,  $z = 60$ ) and wherein the  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2$  has a mean particle size of about 0.1 to 0.7  $\mu\text{m}$ .

9. A dielectric ceramic according to Claim 1 in which the third sub-component is present.

10. A dielectric ceramic according to Claim 2, wherein the molar ratio of  $(\text{Ba} + \text{Ca})/\text{Ti}$  is about 0.99 to 1.035.

11. A laminated ceramic capacitor having:  
a plurality of dielectric layers containing the dielectric ceramic according to Claim 1;

a plurality of inner dielectric layers comprising Ni or a Ni alloy and existing among a plurality of said dielectric layers; and  
external electrodes in electrical continuity to a plurality of said inner dielectric layers and being on the surface of said ceramic capacitor.

12. A laminated ceramic capacitor according to Claim 11, wherein said external electrodes comprise a sintered layer of conductive metal powder or conductive metal powder and glass frit.

13. A laminated ceramic capacitor having:  
a plurality of dielectric layers containing the  
dielectric ceramic according to Claim 2;

5 a plurality of inner dielectric layers  
comprising Ni or a Ni alloy and existing among a  
plurality of said dielectric layers; and  
external electrodes in electrical  
continuity to a plurality of said inner dielectric layers  
and being on the surface of said ceramic capacitor.

14. A laminated ceramic capacitor according to  
Claim 13, wherein said external electrodes comprise a  
sintered layer of conductive metal powder or conductive  
metal powder and glass frit.

15. A laminated ceramic capacitor having:  
a plurality of dielectric layers containing the  
dielectric ceramic according to Claim 3;

5 a plurality of inner dielectric layers  
comprising Ni or a Ni alloy and existing among a  
plurality of said dielectric layers; and  
external electrodes in electrical  
continuity to a plurality of said inner dielectric layers  
and being on the surface of said ceramic capacitor.

16. A laminated ceramic capacitor according to  
Claim 15, wherein said external electrodes comprise a  
sintered layer of conductive metal powder or conductive  
metal powder and glass frit.

17. A laminated ceramic capacitor having:  
a plurality of dielectric layers  
containing the dielectric ceramic according to Claim 6;

5 a plurality of inner dielectric layers  
comprising Ni or a Ni alloy and existing among a  
plurality of said dielectric layers; and  
external electrodes in electrical  
continuity to a plurality of said inner dielectric layers  
and being on the surface of said ceramic capacitor.

18. A laminated ceramic capacitor according to  
Claim 17, wherein said external electrodes comprise a  
sintered layer of conductive metal powder or conductive  
metal powder and glass frit.

5 19. A laminated ceramic capacitor having:  
a plurality of dielectric layers  
containing the dielectric ceramic according to Claim 9;  
a plurality of inner dielectric layers  
comprising Ni or a Ni alloy and existing among a  
plurality of said dielectric layers; and  
external electrodes in electrical  
continuity to a plurality of said inner dielectric layers  
and being on the surface of said ceramic capacitor.

20. A laminated ceramic capacitor according to  
Claim 19, wherein said external electrodes comprise a  
sintered layer of conductive metal powder or conductive  
metal powder and glass frit.

P/1071-814

DIELECTRIC CERAMIC COMPOSITION AND  
LAMINATED CERAMIC CAPACITOR USING THE SAME

ABSTRACT OF THE DISCLOSURE

Provided is a highly reliable laminated ceramic capacitor in which decrease of dielectric constant under a high electric field is small and which satisfies the B-grade and X7R grade characteristics, using Ni for the inner electrodes, wherein the dielectric material contains about 0.2 to 5.0 parts by weight of  $\text{Li}_2\text{O}-(\text{Si}, \text{Ti})_2\text{-MO}$  oxides (MO is at least one of the compounds of  $\text{Al}_2\text{O}_3$  and  $\text{ZrO}_2$ ) or  $\text{SiO}_2\text{-TiO}_2\text{-XO}$  oxides (XO is at least one of the compounds of BaO, CaO, SrO, MgO, ZnO and MnO) relative to 100 parts by weight of a principal component represented by  $(\text{Ba}_{1-x}\text{Ca}_x\text{O})_m\text{TiO}_2 + \alpha\text{Re}_2\text{O}_3 + \beta\text{MgO} + \gamma\text{MnO}$  ( $\text{Re}_2\text{O}_3$  represents at least one of  $\text{Y}_2\text{O}_3$ ,  $\text{Gd}_2\text{O}_3$ ,  $\text{Tb}_2\text{O}_3$ ,  $\text{Dy}_2\text{O}_3$ ,  $\text{Ho}_2\text{O}_3$ ,  $\text{Er}_2\text{O}_3$  and  $\text{Yb}_2\text{O}_3$ ).

FIG. 1

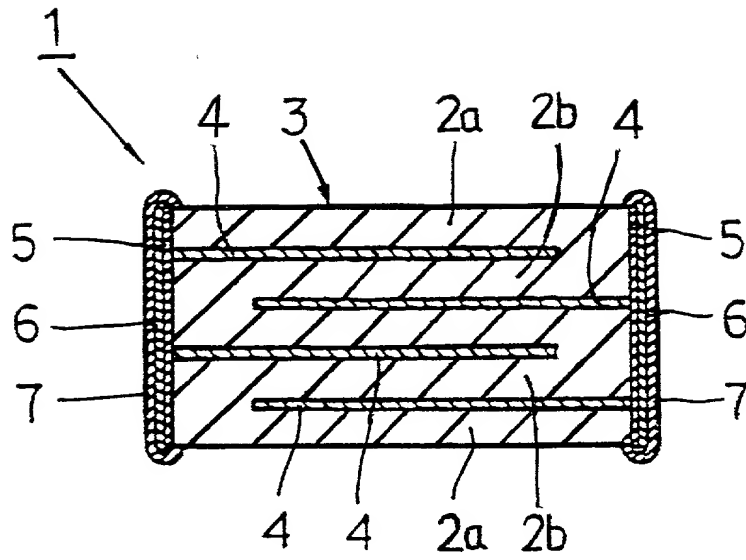


FIG. 2

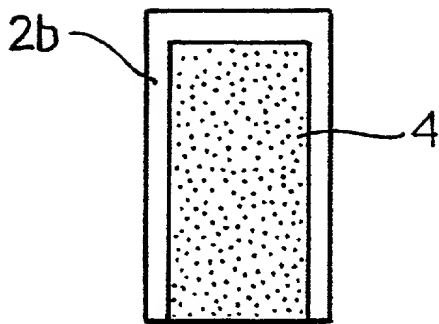
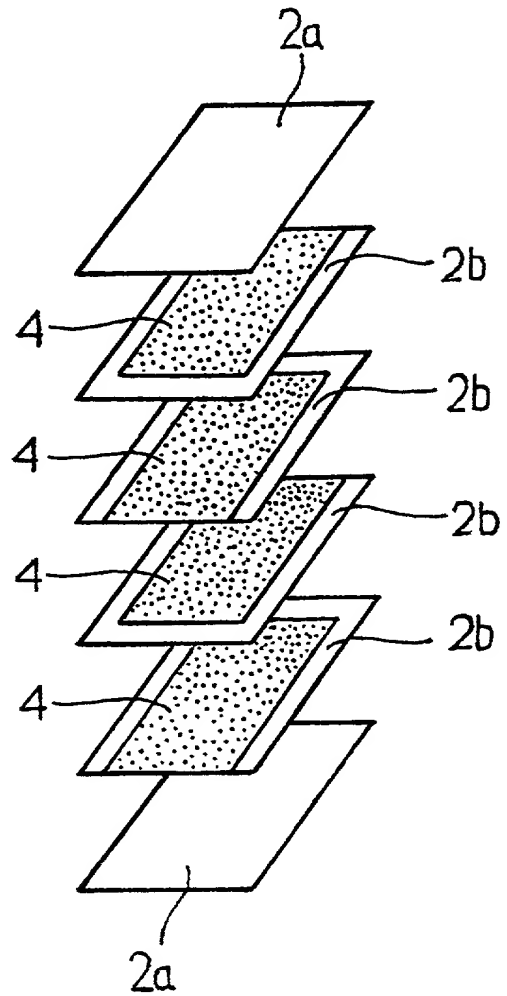


FIG. 3



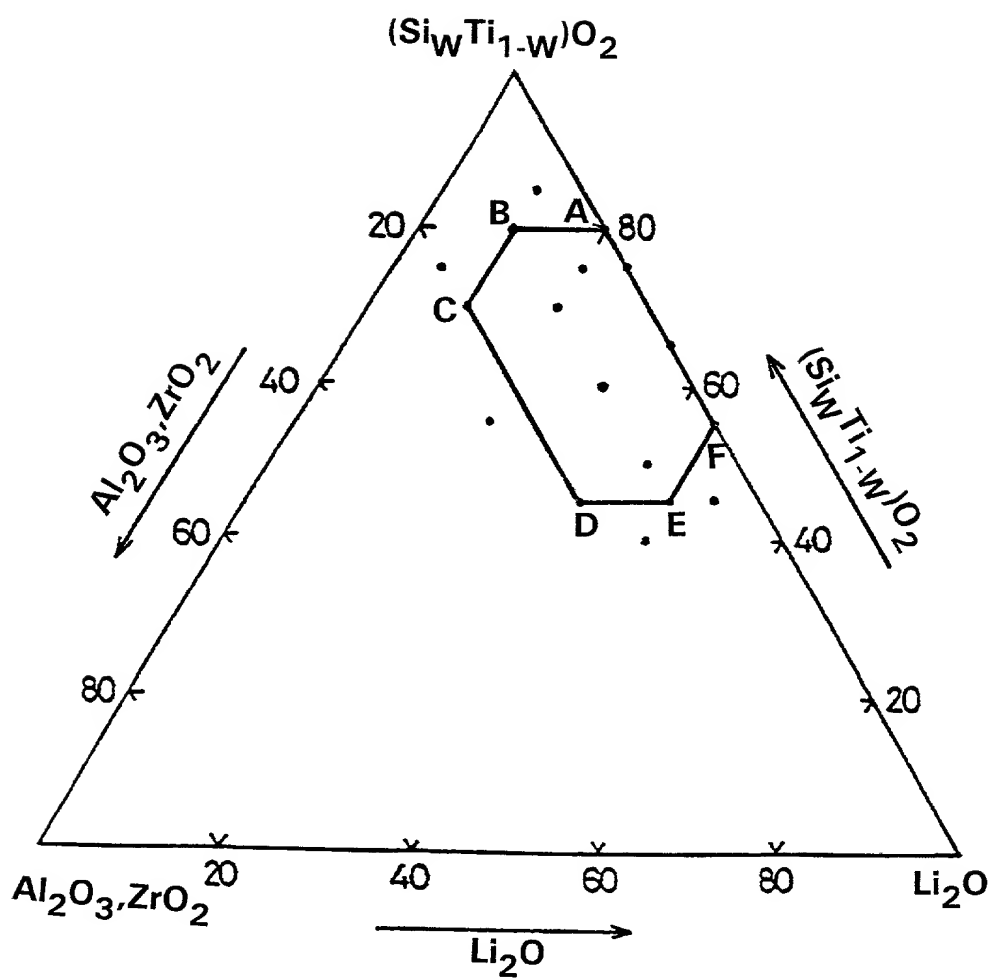


FIG. 4

669080" 886651E60

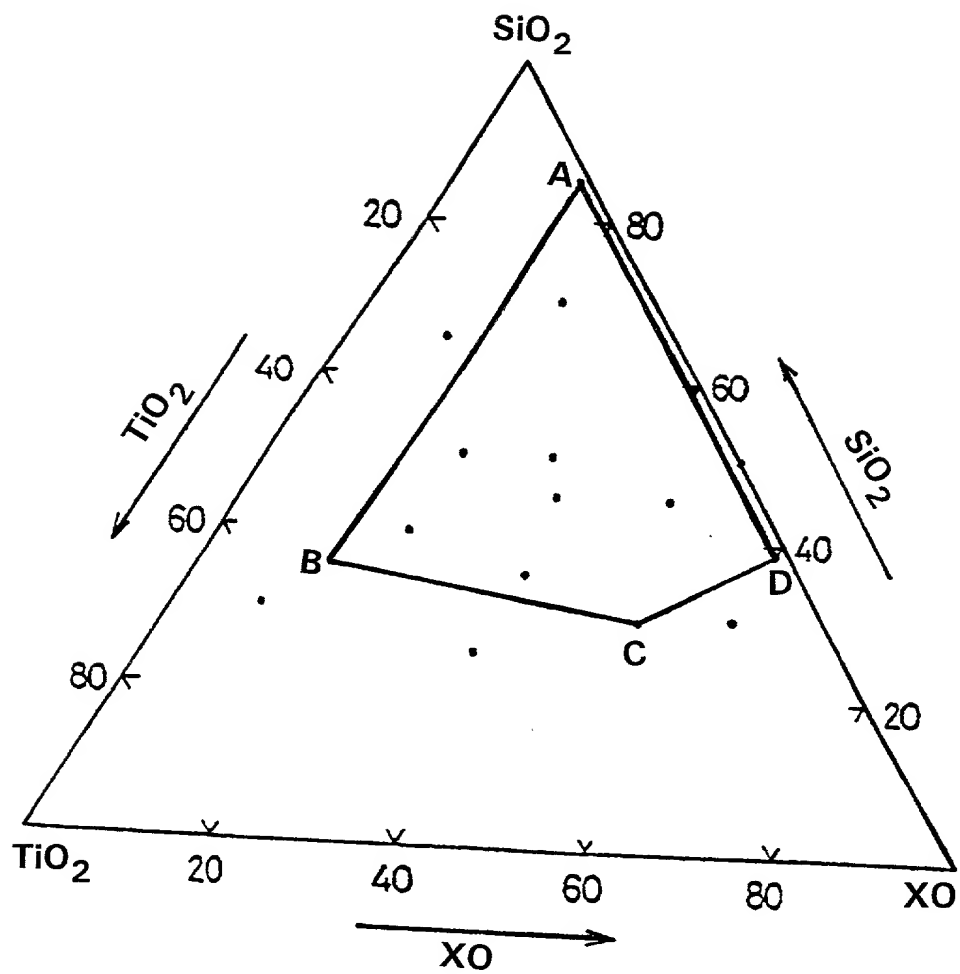


FIG. 5

659030" 88669E60

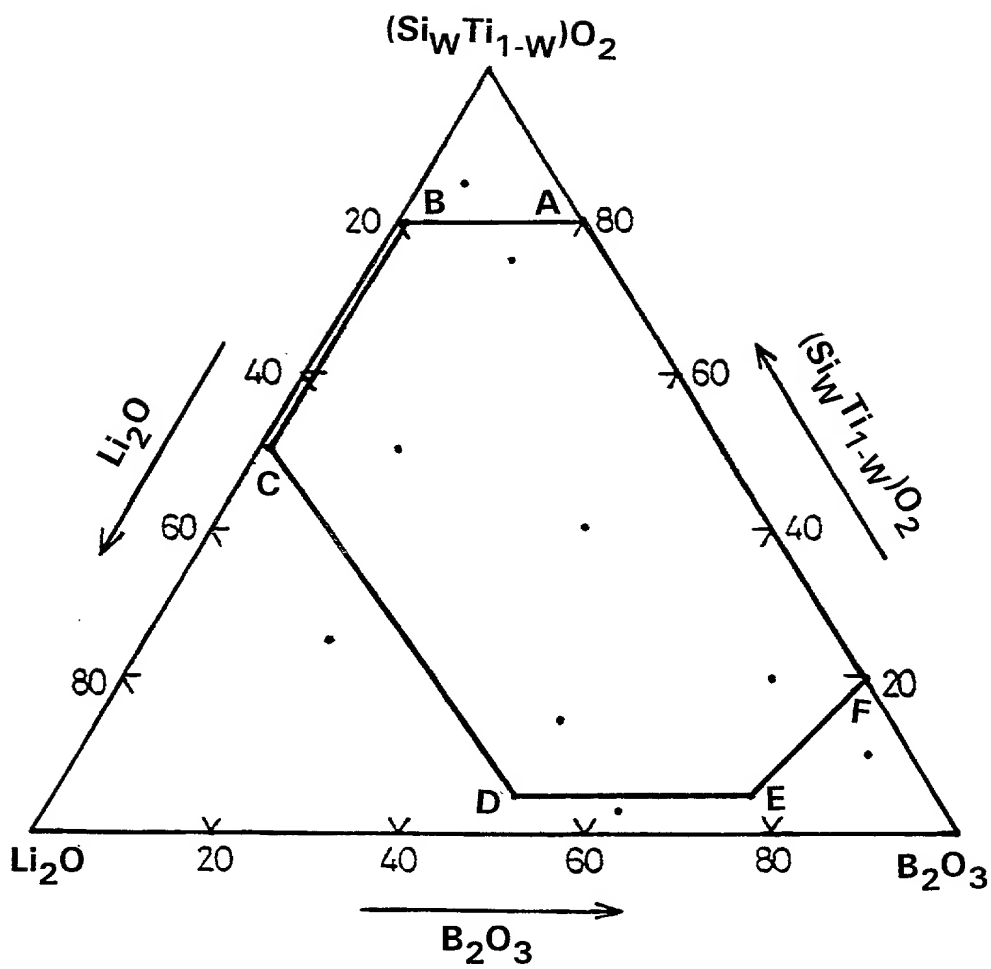


FIG. 6



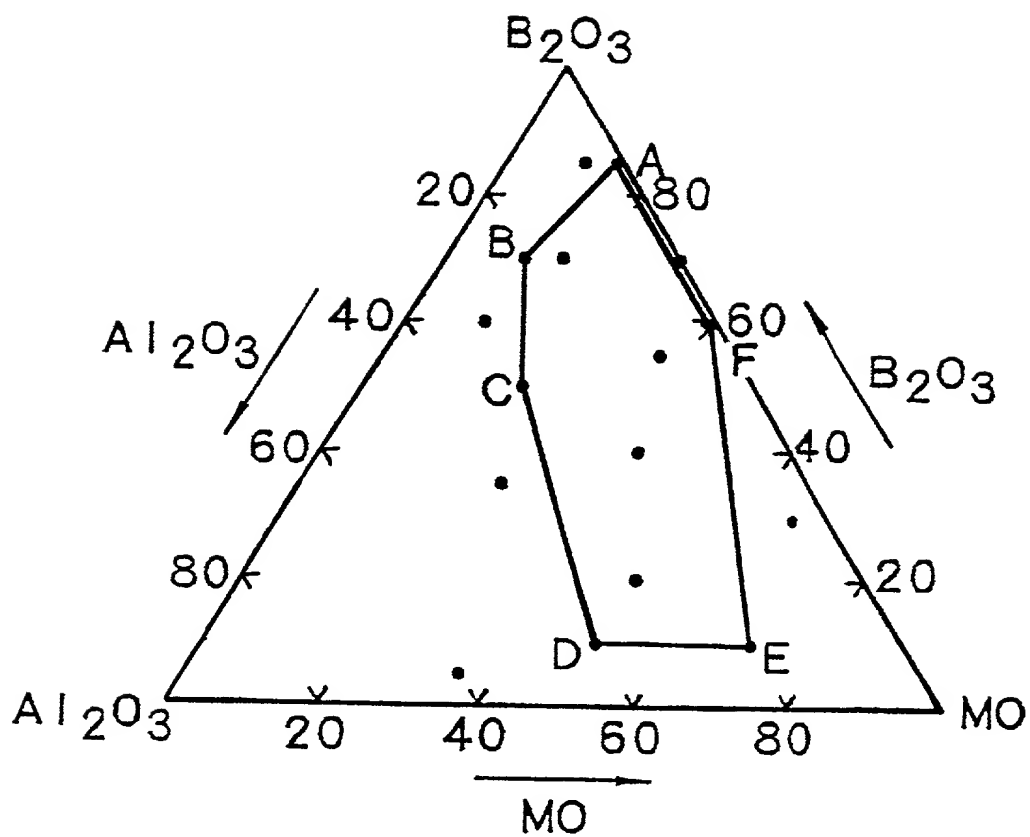


FIG. 7

UNITED STATES OF AMERICA  
COMBINED DECLARATION AND POWER OF ATTORNEY FOR PATENT APPLICATION

OFGS FILE NO.  
P/1071-814

As a below named inventor, I hereby declare that: my residence, post office address and citizenship are as stated below next to my name; that I verily believe that I am the original, first and sole inventor (if only one name is listed below) or a joint inventor (if plural inventors are named) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

**DIELECTRIC CERAMIC COMPOSITION AND LAMINATED CERAMIC CAPACITOR USING THE SAME**

the specification of which is attached hereto, unless the following box is checked:

☐ was filed on \_\_\_\_\_ as United States patent Application Number or PCT International patent application number \_\_\_\_\_ and was amended on \_\_\_\_\_ (if any).

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose all information known to be material to patentability in accordance with Title 37, Code of Federal Regulations, §1.56.

I hereby claim priority benefits under Title 35, United States Code §119 of any foreign application(s) for patent or inventor's certificate or United States provisional application(s) listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

Prior Foreign or Provisional Application(s)

COUNTRY	APPLICATION NUMBER	DATE OF FILING (day, month, year)	PRIORITY CLAIMED UNDER 35 U.S.C. 119
Japan	10-227202	August 11, 1998	YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>
Japan	10-227203	August 11, 1998	YES <input checked="" type="checkbox"/> NO <input type="checkbox"/>
			YES <input type="checkbox"/> NO <input type="checkbox"/>

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, §1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application.

UNITED STATES APPLICATION NUMBER	DATE OF FILING (day, month, year)	STATUS (patented, pending, abandoned)

I hereby appoint customer no. 2352 OSTROLENK, FABER, GERB & SOFFEN, LLP, and the members of the firm, Samuel H. Weiner - Reg. No. 18,510; Harold Einhorn - Reg. No. 20,345; Robert C. Faber - Reg. No. 24,322; Edward A. Meilman - Reg. No. 24,735; Stanley H. Lieberstein - Reg. No. 22,400; Steven I. Weisburd - Reg. No. 27,409; Max Moskowitz - Reg. No. 30,576; Stephen A. Soffen - Reg. No. 31,063; James A. Finner - Reg. No. 30,173; William O. Gray, III - Reg. No. 30,944; Louis C. Dujmich - Reg. No. 30,625 and Douglas A. Miro - Reg. No. 31,643, as attorneys with full power of substitution and revocation to prosecute this application, to transact all business in the Patent & Trademark Office connected therewith and to receive all correspondence.

SEND CORRESPONDENCE TO: **OSTROLENK, FABER, GERB & SOFFEN, LLP** DIRECT TELEPHONE CALLS TO:  
1180 AVENUE OF THE AMERICAS  
NEW YORK, NEW YORK 10036-8403 (212) 382-0700  
CUSTOMER NO. 2352

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

FULL NAME OF SOLE OR FIRST INVENTOR <b>Nobuyuki WADA</b>		INVENTOR'S SIGNATURE	DATE
RESIDENCE (City and either State or Foreign Country) <b>Yasu-gun, Shiga-ken, Japan</b>		COUNTRY OF CITIZENSHIP <b>Japan</b>	
POST OFFICE ADDRESS <b>c/o (A170) Intellectual Property Department, Murata Manufacturing Co., Ltd., 26-10, Tenjin 2-chome, Nagaokakyo-shi, Kyoto-fu 617-8555, Japan</b>			
FULL NAME OF SECOND JOINT INVENTOR (IF ANY) <b>Masamitsu SHIBATA</b>		INVENTOR'S SIGNATURE	DATE
RESIDENCE (City and either State or Foreign Country) <b>Kyoto-shi, Kyoto-fu, Japan</b>		COUNTRY OF CITIZENSHIP <b>Japan</b>	
POST OFFICE ADDRESS <b>c/o (A170) Intellectual Property Department, Murata Manufacturing Co., Ltd., 26-10, Tenjin 2-chome, Nagaokakyo-shi, Kyoto-fu 617-8555, Japan</b>			
FULL NAME OF THIRD JOINT INVENTOR (IF ANY) <b>Takashi HIRAMATSU</b>		INVENTOR'S SIGNATURE	DATE
RESIDENCE (City and either State or Foreign Country) <b>Yasu-gun, Shiga-ken, Japan</b>		COUNTRY OF CITIZENSHIP <b>Japan</b>	
POST OFFICE ADDRESS <b>c/o (A170) Intellectual Property Department, Murata Manufacturing Co., Ltd., 26-10, Tenjin 2-chome, Nagaokakyo-shi, Kyoto-fu 617-8555, Japan</b>			

☒ CONTINUED ON PAGE 2

